Contents lists available at ScienceDirect



Arabian Journal of Chemistry



journal homepage: www.ksu.edu.sa

Poly ether block Amide/Polyvinyl Alcohol/ MgO nanocomposite membranes: Selectivity for CO₂ and CH₄ gases

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ARTICLE INFO

ABSTRACT

Keywords: Polyether block amide Polyvinyl alcohol MgO nanoparticles Molecular dynamics simulations, Permeability One of the methods of improving mixed matrix membranes is the use of nanoparticles and compounds containing hydroxyl and carboxyl groups, which can be a suitable choice to help more permeability of gases. In this study, a mixed matrix membrane comprising polyether block amide/polyvinyl alcohol (Pebax/PVA) and magnesium oxide (MgO) nanoparticles was fabricated via solution casting. The Pebax/PVA membrane with MgO loadings of 10-15 % at varying PVA weight ratios (0, 20, 50, 80 %) was evaluated for CH₄ and CO₂ gas separation performance. Characterization via Fourier transform infrared (FTIR), X-ray diffraction (XRD) and field emission scanning electron microscopy (FESEM) revealed the nanoparticles well-dispersed within the polymer matrix, with surface roughness increasing with MgO addition. XRD analysis indicated stronger interaction between MgO and PVA chains versus Pebax. Peaks at \sim 42, 62° suggest nanoparticles lodged between polymer strands. Variables assessed as independents impacting CH₄ and CO₂ permeability included PVA content, MgO loading, pressure and temperature. ANOVA showed the quadratic model best fitted correlations between variables and responses, Experimental data vielded the formulation with optimum selectivity, Molecular dynamics simulation (MDS) via Materials Studio estimated CH₄ and CO₂ diffusion through selected membranes. Simulated results matched experimental data well. Relative to prior separation data and outcomes herein, the synthesized nanocomposite membrane proved highly effective, promising potential for diverse gas mixtures. Membrane permeabilities were also evaluated.

1. Introduction

Rising global temperatures due to population growth, economic development and increasing energy consumption have made selective CO_2 removal a pressing global challenge(Dong et al., 2022; Norby and Luo, 2004). Substantial research shows that CO_2 emissions from these driving factors are the primary cause of irreversible climate change, with fossil fuels being the most consumed energy source worldwide despite their emissions. In recent decades, polymer membranes have gained prominence for gas separations like H₂/CO₂, CO_2/N_2 , and CO_2/CH_4 due to advantages such as availability, mechanical robustness, and low energy operation(Coronas, 2022; Samuel J. Edens, Michael J. McGrath, Siyu Guo, Zijuan Du, Hemin Zhou, Lingshan Zhong, Zuhao Shi, Jieshuo Wan, Thomas D. Bennett, Ang Qiao, Haizheng Tao, n.d.; Sun et al., 2023). Membrane separation and CO_2 absorption have attracted scientific interest for reducing carbon dioxide emissions and excessive fossil

fuel usage amid growing energy demands. Compared to traditional processes like absorption, extraction and cryogenic distillation, which consume vast energy and incur high costs, membrane separation offers a simpler, scalable design with lower operating expenses(Aydin et al., 2023; Dai et al., 2023). The application of nanotechnology in membrane science for gas separation has created a novel class of nanoengineered materials. Polymer matrix properties within these membranes are modified to enhance separation and filtration performance. While crosslinking, polymer blending, surface alteration, thermal treatment and ligand immobilization have traditionally been employed, mixed matrix membranes incorporating nanofillers into the polymer structure show promising potential as a cost-effective solution(Chakrabarty et al., 2022; Luo et al., 2022). Nanocomposite membranes have received significant attention due to improved selectivity and permeability in gas separation applications relative to selectivity(Clarizia and Bernardo, 2022; Surva Murali et al., 2010; Wang et al., 2023). In CO₂/CH₄ separation,

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https://doi.org/10.1016/j.arabjc.2023.105586

Received 2 March 2023; Accepted 24 December 2023

Available online 25 December 2023

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Table 1

Chemical characteristics of the materials used.

	Pebax	PVA	MgO
Molecular weight (g/mol) Melting point (°C)	- 174-134	86/09 230	40/3044 -
Density (g/cm3)	01/303	01/19	03/58

Table 2

	Independe	nt variables	s and related	levels in	design of	experiments.
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Independent variables	Unit	Levels				
		Level 1	Level 2	Level 3	Level 4	
A: PVA	%	0	20	50	80	
B: MgO	%	0	5	10	15	
C: Pressure	bar	2	4	6	8	
D: Temperature	°C	25	35	45	55	

selectivity refers to preferential permeation of one gas (e.g., CO₂) while effectively blocking the other (e.g., CH₄). Factors like molecular sieving, surface interactions, diffusion kinetics, polymer matrix composition, and operating conditions influence nanocomposite membrane selectivity for these gases(Garcia-Martinez et al., 2023; Martinez et al., 2022). One of the principal challenges in membrane technology is balancing selectivity against permeability, commonly known as the Robeson upper bounds. Robeson's limits delineate the theoretical performance limitations of polymeric membranes with respect to selectivity and permeability for various gas pairs. Generally, improving selectivity tends to decrease permeability and vice versa due to factors such as chain packing density, free volume availability, adsorption strength and solubility selectivity, and polymer chain rigidity(Ahmad et al., 2023; Ghanbari et al., 2023). One of the highly promising approaches is the use of mixed matrix membranes (MMMs). Here, an organic polymer matrix, offering flexibility and ease of processing, is combined with inorganic or organic fillers like zeolites, metal-organic frameworks (MOFs), or nanoparticles which impart enhanced selectivity and permeability. The selected filler material, loading concentration within the matrix, and interfacial interactions between polymer and filler can influence the balancing of selectivity versus permeability in MMMs(Cheng et al., 2023; Ebadi et al., 2021; Kalantari et al., 2020). The use of Magnesium oxide (MgO) nanoparticles in a polymer matrix to create mixed matrix membranes (MMMs) is a common approach to increase gas separation performance(Zainuddin et al., 2023). MgO nanoparticles offer several advantages, including high surface area, thermal stability, and chemical compatibility with various polymer matrices.

So far, polymers such as polysulfone (PSF), polyether sulfone (PES), intrinsically microporous polymers (PIMs) and poly ether-block amide (Pebax) have been studied as polymer matrices for MMM membranes (Al-Rowaili et al., 2023; Ding et al., 2023). Meanwhile, Pebax copolymer has been investigated due to its unique combination of permeability and selectivity, and tunable size for various gas separation applications, including CO₂ absorption, natural gas purification, biogas upgrading, and hydrogen recovery(Isanejad and Mohammadi, 2018; Miri et al., 2020). This copolymer is a family of thermoplastic elastomers that includes a block of soft parts (rubber like polyether) and hard parts (glass like polyamide) that cause gas permeability without losing selectivity and mechanical stability(Zhang et al., 2022).

Fabrication technique is a suitable alternative for improving the properties of mixed matrix membranes due to its simplicity, reproducibility, commercial feature and cost-effectiveness. On the other hand, polymers with hydroxyl and carboxyl groups such as glycerol (Gl), poly (ethylene glycol) (PEG) and poly (vinyl alcohol) alcohol (PVA) are suitable candidates for combination with Pebax membranes(Nobakht and Abedini, 2022; Vatanpour et al., 2023). Studies have shown that adding Pebax to PVA matrix, in addition to forming a composite membrane with gas separation properties, can also reduce the brittleness of pure polymers by forming a defect-free polymer layer with a thin thickness(Ebadi et al., 2021; Kheirtalab et al., 2020). Due to the interaction between the negative charge of oxygen (atoms of carbonyl and hydroxyl groups) with the central carbon with the positive charge of CO_2 through the interaction based on Lewis's acid, it can help to penetrate more CO_2 .

Reza et al. in 2023 reported the high-performance separation of CO₂ gas using a mixed membrane of Pebax/maltitol/ZIF-8 with high efficiency. Gas permeability analysis at 30 $^\circ C$ and 10 bar showed that the Pebax/maltitol/ZIF-8 membrane exhibited the highest CO2 permeability at 429.57 Barrer. Additionally, the highest selectivity values for CO2/N2 and CO_2/CH_4 separation were reported as 69.31 and 26.59, respectively, at 30 °C and 10 bar(Bakhtin et al., 2023). Sanaipour et al. investigated the effect of combining cellulose acetate with Pebax to enhance the properties of CO₂ separation using the casting method and evaluated its performance in gas separation. The permeability results have shown that the permeability and selectivity of CO2 in the cellulose acetate/Pebax composite membrane increased by 25 % and 59 %, respectively, compared to pure cellulose acetate(Sanaeepur et al., 2019). In 2018, Azizi et al. reported the performance of CO₂/CH₄ separation using a Pebax/PEG-200 mixed membrane. The results showed that the Pebax/ PEG-200 mixed membrane with a 40 % weight loading exhibited CO₂ permeability and CO₂/CH₄ selectivity values of 351.65 and 9.17, respectively, compared to pure Pebax(Azizi et al., 2017). In a 2019 study, researchers investigated the use of Pebax nanocomposite membranes with varying weight percentages of aluminum oxide (Al₂O₃) for the separation of CH₄ and CO₂ gases and the determination of their permeation rates. The results demonstrated that Pebax/Al₂O₃ nanocomposite membranes exhibited CO2 permeability and CO2/CH4 selectivity values of 159.27 and 24.73, respectively, at a pressure of 3 bar. Examination of FESEM images revealed the uniform distribution of Al₂O₃ nanoparticles within the polymer matrix, indicating defect-free membrane structures(Farashi et al., 2019).

In this study, MgO nanoparticles were incorporated into a mixed matrix membrane aimed at CO_2 separation. The base polymeric matrix comprised Pebax blended with PVA bearing hydroxyl functionalities at 0, 20, 50 and 80 wt%, fabricated by solution casting. MgO nanoparticles, leveraged as 10 and 15 wt% loads, sought to boost selectivity and permeability. Membrane identification via FTIR, XRD and FESEM characterization was explored. Variables analyzed as independents influencing CH_4 and CO_2 gas permeability encompassed PVA content, MgO loading level, pressure and temperature. Structural insights and the effect of polymer blending on separation performance were garnered from the synthesized alloys. Moreover, molecular dynamics simulations assessed selectivity and diffusion coefficients to illuminate gas transport.

2. Materials and methods

2.1. Materials

The polymeric constituents utilized were polyether block amide branded Pebax-2533(PEBA, Pebax 2533) and polyvinyl alcohol (PVA), purchased from Arkema (France) and Merck (Germany) respectively. Magnesium oxide (MgO) nanoparticles (particle size < 50 nm) and 95 % purity were obtained from USNANO to formulate the nanocomposite membrane and acetic acid (glacial, Reagent Plus (0, 299)) were purchased from Sigma Aldrich. As solvent, dimethylacetamide was selected - a colorless polar liquid. Chemical properties of the materials are delineated in Table 1.

2.2. Methods

2.2.1. Design of experiment (DOE)

In this study, response surface methodology employing a D-optimal design was utilized given all variables were independent with constraints. The Design Expert software (Version 7.0.0, Stat-Ease Inc.,

Table 4 Optimal formulations

optim									
	A	В	С	D	Selectivity index (Theoretical)	Selectivity (α) (Practical)			
#1 #2	5 5	6 12	7 6	27.5 25	20.84 12.78	26.30 15.58			

Minneapolis, MN) facilitated a central composite design(Kazemi et al., 2020). The proportions of PVA and MgO nanoparticles as well as gas pressure and temperature were designated as the independent variables, with CH_4 and CO_2 membrane permeabilities selected as responses. The independents were defined at 4 levels, as delineated in Table 2. Sixteen runs were generated, shown in Appendix Table A. Subsequently, the top three formulas exhibiting the highest attractiveness indices per the model were chosen for further testing and characterization.

2.2.2. Membrane preparation

The polyether block amide/polyvinyl alcohol (Pebax/PVA) membrane was fabricated via the following process: First, a 3 wt% solution was prepared by dissolving 0.3 g of Pebax polymer and PVA at varying weight ratios in 10 cc of dimethylacetamide solvent. The mixture was sonicated at 120 °C to ensure complete dispersion of the polymers. The homogeneous solution was then stirred magnetically at an elevated heat of 12 h to promote uniformity. Next, the obtained solution was cast into a Teflon petri dish and placed in an oven at 75 °C for 12 h to form the desired film. Post-formation, the film underwent thermal treatment in a vacuum oven for 4 h. This final step aimed to remove residual solvent and optimize the membrane's physicochemical properties. The resulting composite membrane was termed Pebax/PVA.

To fabricate the polyether block amide/polyvinyl alcohol/magnesium oxide nanoparticle composite membrane (Pebax/PVA/MgO), 10 and 15 wt% MgO nanoparticles were ultrasonicated in dimethylacetamide solvent at 45 °C for 2 h to ensure uniform dispersion. Subsequently, 0.2 g of the Pebax/PVA polymer mixture was added to the nanoparticle solution and further sonicated at 120 °C. Next, to achieve homogeneous blending, the solution was magnetically stirred at elevated heat for a designated duration. The prepared solution was then cast into a Teflon petri dish and placed in an oven at 75 °C for 12 h to form the membrane film. Post-formation, the film underwent thermal treatment in a vacuum oven for 4 h to extract residual solvent and optimize the membrane's properties. The resulting composite membrane was termed Pebax/PVA/ MgO.

2.3. Membrane characterization

2.3.1. FESEM analysis

The nanocomposite membranes were firstly immersed in liquid nitrogen for 30 s to enable clean splitting into two portions. Both exposed interior surfaces were stub-coated using a double-sided conductive silver adhesive prior to gold sputter-coating via a sputter coater (SCDOOS, Baltic, Switzerland). Cross-sectional micrographs at magnifying ratios were then obtained using a Vega II scanning electron microscope (Tescan, Czech Republic) operated at 20 kV. Secondary electron detection facilitated examination of membrane microstructures(Keshavarz et al., 2020).

2.3.2. XRD analysis

X-ray diffraction (XRD) was used to investigate the XRD patterns of the samples. The analysis was performed using an ICDD Grant Germany instrument, with CuK α radiation ($\lambda = 1.5418$ Å). The scanning range was set from 20 to 60° in steps of 0.05°, while the instrument operated at 40 kV with a current of 30 mA.

2.3.3. Gas separation

The permeability characteristics of PEBA/PVA/MgO membranes to

pure gases (CO_2 or CH_4) were analyzed using a constant pressure mode at various temperatures (25, 35, 45, and 55 °C)(Med, n.d.). The feed side pressures of the gases ranged from 2 to 8 bar, while the permeate side was maintained at 1 atm. The CO2/CH4 mixture gas separation efficiency of the optimal samples was evaluated at 6 or 7 bars and 27.5 or 25 °C (Table 4). The evaluation was conducted using a mixed gas input containing 10 mol% CO2. The separation measurements were carried out using similar mixed gas systems as reported by Khraisheh et al (Khraisheh et al., 2020), with a few minor differences in operational circumstances. In the experiment, a gas mixture of 10 mol% CO2 in CH4 was used to pressurize the feed side of the membrane up to 7 bars, while the permeate side was maintained at atmospheric pressure. The permeate was analyzed using a Varian micro-GC (490-GC Micro-GC) equipped with a PPQ column, heated auto-injector, and backflush option for volatile compounds such as CO₂ and CH₄. The delay time method was used to investigation the permeability of CO₂ and CH₄ gases. This method is the most common test for gas permeability in polymer membranes. In this method, the penetration of gas in the polymer is measured and investigated from zero time until the polymer permeability reaches a constant number. The constant pressure method was used to check the amount of gas seeped through the membrane and to record the flow rate of the passing gas.

The delay time was calculated through equation (1)(Wang et al., 2023):

$$\theta = \frac{l^2}{6D} \tag{1}$$

where θ is the delay time (s), the thickness of the membrane (cm) and the gas diffusion coefficient in the membrane (cm²/s), which is obtained by measuring the slope of the line in the steady state, and the flow rate of the passing gas in terms of time (Q). Next, the gas permeability coefficient in the polymer was calculated according to equation (2):

$$P = \frac{Q.L}{(P1 - P2).A}$$
(2)

where $P(cm^3(STP).cm/cm^2.s. cmHg)$ gas permeability coefficient in polymer, $Q(cm^3(STP)/s)$ gas flow through the membrane, L (cm) membrane thickness, P1 and P2 gas pressure in Upstream and downstream, $A(cm^2)$ are the cross-sectional area of the membrane. The word STP in Barer unit indicates the volume of gas at standard temperature and pressure equal to 273.15 K and 760 Torr. At standard temperature and pressure, one mole of any gas has a volume of 22.4 l. The unit of permeability coefficient in the SI system is expressed according to the following equation:

$$P = \frac{mol}{m^2 s. Pa} \tag{3}$$

By specifying the diffusion coefficient and gas permeability coefficient in the membrane using the dissolution-permeation relationship, the solubility coefficient of the studied gases in each membrane is obtained from equation (4):

$$S = \frac{P}{D}$$
(4)

The optimal selectivity was calculated with the following relation:

$$\alpha = \frac{P_{CO2}}{P_{CH4}} \tag{5}$$

2.3.4. Molecular dynamics simulation

Molecular dynamics is a method to observe atomic and molecular motions on the microscopic scale. According to Newton's formula, MD allows the examination of microscopic movements of systems containing N atoms(Bahreini et al., 2024, 2023):



Fig. 2. FTIR spectra of membranes.

1



Fig. 3. XRD graph of optimal formulations.

$$m_i \frac{\partial^2 r_i}{\partial t^2} = F_i, i = 1 \cdots N.$$
(6)

Eq. (7) states that the forces (Fi) are equivalent to the potential function (V), in which ri and t stand for the center-of-mass position vector related to penetrant i and the time, respectively.

$$F_i = -\frac{\partial V}{\partial r_i} \tag{7}$$

The equations are then solved in small time steps at the same time. The system is monitored for some time while regulating the temperature and pressure, and the coordinates are sent to an external file at scheduled intervals. A represented trajectory of the system is these coordinates as a function of time. Initially, the system typically achieves equilibrium. Numerous microscale features, like diffusion processes in membranes, may then be retrieved from the output file by calculating the average over an equilibrium trajectory. The diffusion coefficient of a gas in an organic solvent, polymer, or clay may be computed by running an MD simulation and calculating the gas's mean square displacement (MSD) in the media. Assuming that the penetrant molecules exhibit random walks in the polymer matrix over extended periods, the mean-square-displacement factor is linear with time, and the diffusion coefficients may be determined utilizing the Einstein formula(Ullal and Spearot, 2014):

$$D = \frac{1}{6N} \lim_{t \to \infty} \frac{d}{dt} \left\langle \sum_{i}^{N} \left[r_i(t) - r_i(0) \right]^2 \right\rangle$$
(8)

Tracking the penetrant's migration $|\mathbf{r}(t)-\mathbf{r}(0)|$ from its initial location allows us to study the motion profile of penetrant gases in the substrate polymer. After that, the slope of a plot of the mean squared displacement versus time t is used to determine the diffusion coefficient D.



Fig. 4. FE-SEM micrographs of samples containing a) 0, b) 20, c) 50 and d) 80 % of PVA.

$$\langle \sum_{i}^{N} \left[r_{i}(t) - r_{i}(0) \right]^{2} \rangle \tag{9}$$

In this regard, the *PEBA* and *PVA* were modeled by putting together ten chains of 30 monomer units as shown in Fig. 1.

The polymer model for Pebax® 2533 and PVA contains 5370 and 2120 atoms, respectively, and the sides of the cubic unit cells measure approximately 29–31 Å. Using the Materials Studio suite of software's Amorphous Cell module, several configurations of polymer chains (depicted in Figure B of the Appendix) were produced and arranged in a cubic space based on Theodorou and Suter's "self-avoiding" random-walk method and the Meirovitch scanning technique, employing periodic boundary conditions (PBC) to model the cubic structure(Meirovitch, 1983). At 1 bar and 298 K, the aim was to generate refined systems approximating the experimental density of the amorphous polymers. In all simulations, Berendsen's method [40] controlled temperature and pressure using a half-life of 0.1 ps (decay constant) and a

pressure scaling constant of 0.1 ps, with a system compressibility of 0.5 GPa-1.

Four CO₂ and CH₄ solute molecules were placed at the center of the simulation space comprising 10 chains of 20 monomers each of the PEBA and PVA blend, to model gas diffusion. A group-based cutoff was employed in this investigation. The COMPASS forcefield described all interactions, using a cutoff value of 12.5 Å. A 3 Å width spline function interpolates the nonbonding interactions from their full value to zero within this range due to computational constraints. Both the cutoff and splining were also modified for long-range effects. For Geometry Optimization the Maximum Iterations was set to 1000.

3. Result and discussion

The 16 formulations were organized according to the design of the experiments. CO_2 and CH_4 permeation of the resulting specimens was then evaluated. Following this, multiple models were employed to fit the data for the two responses (permeation rates). Analysis of variance



Fig. 5. Nanoparticles' dispersion in polymer matrix for a) Pebax20/PVA80/MgO15%, and b) Pebax80/PVA20/MgO10%.



Fig.6. A) the effect of pressure on the permeability of co₂ gas and b) The effect of temperature on the permeability of CO₂ gas of samples containing 0, 20, 50, and 80 % of PVA.

(ANOVA) was used to assess the adequacy of the models and establish a valid and trustworthy relationship between the dependent and independent variables. As the manufactured membranes had a similar thickness range of 40–80 μm , the impact of membrane thickness on the responses was able to be excluded. Table A in the Appendix illustrates the findings for all membrane responses.

3.1. Fourier-transform infrared spectroscopy (FT-IR)

FT-IR was employed to characterization and identify the functional groups in the membranes of composite and nanocomposite structures. The results of this investigation for the specimen membrane are presented in Fig. 2, respectively. In Fig. 2, the observed peaks for the Pebax in the range of 3300 and 2860 cm⁻¹ correspond to the stretching vibrations of N–H and aliphatic C–H groups, respectively. Additionally, absorption peaks appearing in the regions of 1720, 1630, and 1100 cm⁻¹ correspond to the C = O, H-N-C = O, and C-O bonds, respectively. The curves in Fig. 2 reveal peaks for PVA in the range of 3300–3500 cm⁻¹, indicative of the stretching vibrations of O–H bonds resulting from

intermolecular and intramolecular hydrogen bonding. Moreover, observed absorption peaks in the regions of 1742 and 1140 cm^{-1} are associated with the C = O and C-O bonds arising from the remaining acetate groups in the structure. The absorption peak at 1627 cm^{-1} indicates carbonyl groups, while the peak at 1147 cm^{-1} signifies the presence of crystalline regions in the PVA chain structure formed due to symmetric stretching of C-C or C-O bonds resulting from intramolecular hydrogen bonding. As seen in Fig. 2, in the FTIR spectrum of the Pebax/ PVA membrane, the positions of the peaks have slightly changed due to the interaction between the Pebax and PVA. This can be attributed to the suitable interaction between the carbon and nitrogen atoms of the Pebax and the hydrogen atoms of PVA. The positional shift of H-N-C = O in the Pebax from 1600 to 1630 cm^{-1} in the Pebax/PVA composite membrane is observed. Furthermore, the stretching vibration of O-H in the polyether block amide has shifted from 3300 to 1325 cm⁻¹ in the mixed Pebax/PVA membrane(Klepić et al., 2020; Martínez-Izquierdo et al., 2019; Mina Kheirtalab, Reza Abedini, 2022; Wong et al., 2021).



Fig.7. A) the effect of pressure on the permeability of ch₄ gas and b) The effect of temperature on the permeability of CH₄ gas of samples containing 0, 20, 50, and 80 % of PVA.



Fig. 8. A response surface plot depicting the influence of A to D variables on CO2 permeability.



Fig. 9. The effect of nanoparticles on the permeability of CO₂ gas in Pebax/PVA/MgO nanocomposite membrane of samples containing 0, 20, 50, and 80 % of PVA.

3.2. X-ray diffraction

The interaction between nanoparticles and polymer chains may cause the nanoparticles to change crystalline form. The change in crystal size and form can be detected by an X-ray diffraction test. The structures of Pebax 1657 polymer, Pebax/PVA composite membrane, and Pebax/ PVA/MgO nanocomposite membrane were investigated using X-ray diffraction (XRD). Fig. 3 illustrates the X-ray diffraction patterns of the fabricated membranes. All polymers exhibit prominent peaks in the range of around 24°, indicative of small, distributed crystals within the S. Ebrahimi et al.



Fig. 10. A response surface graph depicting the influence of A to D variables on CH4 permeability.



Fig. 11. MSD (Å) vs Time (ns) for a) CH₄ and b) CO₂ at different percentages of PVA.

Table 3Diffusion coefficients of CH4 and CO2.

PVA content (%)	Diffusion coefficient $\times 10^5$ (m ² . s ⁻¹)		Gas selectivity
	CH4	CO ₂	
0	21.43	1.25	17.15
20	21.95	1.85	11.86
50	20.65	3.22	6.42
80	15.90	4.03	3.94
100	12.33	6.52	1.89

*Gas selectivity is the ratio of CH4 to CO2 diffusion coefficients.

polymeric membrane composition. With the addition of 10 % by weight of MgO nanoparticles to the polymeric blend of Pebax/PVA, a reduction in peak intensity in the 24° regions is observed. The decreasing trend in the composite and nanocomposite membranes suggests a reduction in

the crystallinity of the membranes(Kheirtalab and Reza Abedini, 2022; Kheirtalab and Reza Abedini, 2020). Moreover, the addition of MgO nanoparticles to the polymer blend has led to the emergence of peaks in the 42° and 62° regions. This phenomenon could be attributed to the placement of MgO nanoparticles between the polymer chains, preventing them from closely packing and linking polymer particles together. On the other hand, the addition of MgO nanoparticles has resulted in broader peaks, indicating a decrease in crystalline properties and facilitating the flexibility of the nanocomposite membrane. In fact, MgO, by reducing the crystalline portion of the membranes and enhancing the polymer chain flexibility, contributes to the improvement of the gas transport properties of CO_2 . Interaction between nanoparticles and polymer chains may cause changes in the crystalline shape and size of the nanoparticles, which can be detected through X-ray diffraction experiments.



Fig. 12. Gas diffusion coefficients for a) CH₄ and b) CO₂ obtained from molecular dynamics simulation and c) CH₄ and d) CO₂ gas permeabilities obtained from experimental data.

3.3. Study of morphology

The morphological investigation of composite membranes with different ratios, including Pebax100/PVA0%, Pebax80/PVA20%, Pebax50/PVA50%, and Pebax20/PVA80%, was conducted using fieldemission scanning electron microscopy (FE-SEM). FE-SEM images of the fabricated membranes are presented in Fig. 4. a-c. As observed in Fig. 4. a. Pebax membranes exhibit a texture structure with irregular distribution, and spherical-shaped pores are also visible(Nobakht and Abedini, 2022). In the images of Pebax80/PVA20% composite membrane (Fig. 4. b), a heterogeneous structure with irregular distribution is evident. This heterogeneity can be attributed to the immiscibility of Pebax and PVA membranes with each other. Furthermore, in Fig. 4.c & d, as the PVA content increases, the cross-sectional surface of the samples becomes smoother due to improved compatibility between the two polymers. With an increase in PVA content, Pebax chains are adequately dispersed, forming a homogeneous phase. The more uniform phases lead to increased gas permeability and enhanced selectivity due to reduced entanglement. The smooth surface and improved compatibility between the polymers contribute to the dispersion of Pebax chains, forming a more uniform phase(Chen et al., 2023). This uniformity results in enhanced gas permeability and increased selectivity due to reduced entanglement.

In the images of Pebax20/PVA80/MgO15% and Pebax80/PVA20/ MgO10% nanocomposites in the Fig. 5, it is evident that the addition of MgO nanoparticles during the membrane preparation stages enhances the texture and structure of the membrane compared to the Pebax/PVA composites. The surface roughness increases, and the nanoparticles are well-dispersed in the polymer matrix. The resulting membrane exhibits a uniform distribution with a coherent structure and regular holes, contributing to the overall improvement in membrane performance. The images also reveal that the nanoparticle size for Pebax20/PVA80/ MgO15% is 302 nm, and for Pebax80/PVA20/MgO10% is 285 nm. This increase suggests swelling, exfoliation, and dispersion of nanoparticles within the polymer chains. Additionally, the strong interaction between nanoparticles and the polymer substrate, coupled with the reduction of the crystalline phase, is observed as the driving force behind the increased permeability and gas separation efficiency.

3.4. Analysis of gas

According to previous studies, CO_2 permeability increases with increasing pressure in polymer membranes. While for light gases such as CH₄, this trend is decreasing or unchanged. According to the results of the investigations, the permeability of CO_2 gas is higher than that of CH₄. The greater permeability of CO_2 compared to CH₄ in Pebax/PVA



Fig. A1. Cross-sectional images of some membrane.

membrane can be attributed to the interaction of CO_2 and the softening effect of CH4 on the polymer. In addition, another reason for the higher permeability of CO_2 compared to CH₄ is the high critical temperature of CO_2 compared to CH₄ gas. In terms of molecular size, carbon dioxide is smaller than the studied methane gas and has a higher condensability. The results of CO_2 and CH₄ gas permeation at pressures of 2, 4, 6 and 8 bar and temperatures of 25, 35, 45 and 55 °C by Pebax/PVA mixed membrane with different weight ratios of PVA are shown in Figs. 6 and 7. As can be seen in Figs. 5 and 6, gas permeation values through the membrane increase with increasing pressure due to increasing driving force caused by mass transfer and solubility of gases. By increasing the pressure from 2 to 8 bar, the permeability of CO_2 and CH_4 gas has increased. In the rubber membrane, the permeability of light and nonpolar gases such as methane is independent of pressure and remains constant with increasing pressure, but the permeability of condensable gases increases with increasing pressure. This increase can be related to



Fig. B1. Optimal configuations for a, b) 0, c, d) 20, e, f) 50, g, h) 80 and i, k) 100 % PVA; left side for CO₂ and right side for CH₄.

the greater affinity of CO_2 with the polar ether groups of Pebax, which increases the CO_2 absorption in the membrane with the increase in pressure, followed by an increase in solubility. The investigation of changes in permeability with temperature for the Pebax/PVA nanocomposite membrane is shown in Fig. 6-b and Fig. 7-b. As can be seen, the permeability increases as the temperature increases to 55 degrees Celsius. The temperature dependence of permeation for CO_2 and CH_4 gases in the membrane is probably due to the double effect of permeation and solubility(Feng et al., 2023). The measured CO_2 permeability of the membranes was between, 53.569 to 315.440. The most suitable model to fit the relationships between the individual variables and Carbon dioxide permeability is a derived quadratic, according to the analysis of variance (ANOVA) (Table C in Appendix). The model's F-value (19.26) suggests that it is significant. Figure C in the Appendix compares the experimental results to predicted CO_2 permeability values. The normalized graphs of the findings are provided in graph a in Figure C in the Appendix for faster and more effective comparisons. Based on the actual value of the



Fig. C1. Linear correlation plot between (a) normal % probability and externally studentized residual, (b) actual and predicted values, (c) externally studentized residual and run number (d) and externally studentized residuals and predicted values for CO₂ permeability results.

findings, graph b in Figure C in the Appendix presents the model's anticipated value of the test results. The residual value in terms of formulations is shown in graph c in Figure C in the Appendix (16 formulations in this study). The residual value (the deviation for both the actual values and the values obtained from the model) is represented in terms of the predicted value in graph d in Figure C in Appendix. The Percentage error for Carbon dioxide permeability among all experimental tests varied between -5.33 percent and +5.33 percent, as seen on the graph's y-axis. As a result, the model is best suited because the discrepancy across the experimental and anticipated values is quite small. The formulation should be skipped if one of the effects falls beyond this range.

Fig. 8 depicts the results of the CO2 permeability test. As illustrated in Fig. 8, the effect of PVA percentage on CO₂ permeation is slightly complex and differs from high pressure and temperature at low pressures and temperatures. Two factors control the penetration of gas into the membrane. One is the polar interactions between CO₂ and PVA molecules that cause more gas molecules to dissolve inside the membrane, thereby increasing the gas permeation. On the other hand, with increasing the percentage of PVA, the possible crystal points inside the membrane increase, which as a barrier prevents the penetration of gas from the membrane. The outcome of these two factors determines the gas permeation through the membrane according to the conditions. MgO nanoparticles also have a great effect on decreasing the CO_2 permeability (graph *a* in Fig. 8), MgO nanoparticles are on the nanometric scale, interact with polymer chains greatly and act as a barrier18. Fig. 8 illustrates that the CO_2 permeability increases as the gas pressure increases. This event indicates that tiny molecules of gases were capable of entering and transferring via the polymer chain, increasing CO_2 permeability. By increasing the gas temperature, molecular movements increase and cause more gas to transfer through the membrane. In addition, the warmer gas raises the membrane temperature and increases the free volume of the polymer chains. Gas molecules pass more easily through polymer chains with higher free volume.

As the study shows that the independent variables influence CO_2 permeability. Eq. (10) displays the mathematical correlation for both CO_2 permeability and the A to D variables acquired from the regression study.

$$CO_{2} permeability = 120.28 - 40.80^{*}A - 6.79^{*}B - 10.73^{*}C + 11.46^{*}D - 36.14^{*}AB - 16.17^{*}AC - 15.58^{*}AD + 43.65^{*}BC + 37.85^{*}C^{2}$$
(10)

The results of examining the selectivity of CO_2 and CH_4 gas at pressures of 2, 4, 6, and 8 bar and temperatures of 25, 35, 45, and 55 °C by Pebax/PVA mixed membrane with different weight ratios of PVA are



Fig. D1. Linear correlation plot between (a) normal % probability and externally studentized residual, (b) actual and predicted values, (c) externally studentized residual and run number (d) and externally studentized residuals and predicted values for CH₄ permeability results.

 Table A1

 Variables and measured responses for designed experiments.

Run	PVA (%), A	MgO (%), B	Pressure (MPa), C	Temperature (°C), D	CO ₂ permeability	CH4 permeability
1	0	0	2	25	170.636	22.934
2	50	5	8	45	116.598	29.716
3	20	10	8	25	180.290	22.651
4	0	10	6	45	170.561	35.222
5	50	0	6	55	108.271	24.633
6	0	5	4	35	176.740	25.168
7	20	5	2	55	212.541	29.446
8	0	15	8	55	315.440	28.583
9	80	10	4	55	79.246	14.258
10	80	0	8	35	100.411	17.690
11	80	15	2	45	53.569	12.769
12	20	0	4	45	160.003	22.651
13	20	15	6	35	150.572	22.764
14	80	5	6	25	83.468	12.956
15	50	10	2	35	135.905	23.217
16	50	15	4	25	87.395	17.869

presented in Fig. 9. As can be seen, permeability and selectivity increase at higher pressures due to the strengthening of the driving force and softening effect. Examining the values obtained from the Pebax/PVA nanocomposite membrane in the selectivity study showed that, as a

result of the compatibility of the polymer surface, the polymer chains can create gaps or narrow seams due to the strong interaction around PVA, which increases the selectivity. Another reason for the simultaneous increase in permeability and selectivity is the absence of non-

Table B1

ANOVA for CO₂ permeability.

Source	Sum of Squares	Df	Mean Square	F-value	p-value	
Model	59369.09	9	6596.57	19.26	0.0009	significant
A-PVA	5301.51	1	5301.51	15.48	0.0077	
B-MgO	90.72	1	90.72	0.2648	0.6252	
C-Pressure	238.22	1	238.22	0.6954	0.4363	
D-Temperature	691.44	1	691.44	2.02	0.2052	
AB	1140.00	1	1140.00	3.33	0.1179	
AC	265.89	1	265.89	0.7762	0.4122	
11AD	672.62	1	672.62	1.96	0.2107	
BC	3261.89	1	3261.89	9.52	0.0215	
C^2	4527.07	1	4527.07	13.22	0.0109	
Residual	2055.29	6	342.55			
Cor Total	61424.37	15				

Table (21
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ANOVA for CH₄ permeability.

Source	Sum of square	DF	Mean of Squares	F-value	Prob > F	
Model	564.53	9	62.73	8.36	0.0089	significant
A-PVA	211.13	1	211.13	28.14	0.0018	
B-MgO	2.90	1	2.90	0.3860	0.5573	
C-Pressure	32.17	1	32.17	4.29	0.0838	
D-Temperature	75.71	1	75.71	10.09	0.0192	
AC	11.27	1	11.27	1.50	0.2662	
BC	34.70	1	34.70	4.63	0.0750	
CD	19.27	1	19.27	2.57	0.1601	
A^2	22.86	1	22.86	3.05	0.1315	
B^2	49.21	1	49.21	6.56	0.0428	
Residual	45.01	6	7.50			
Cor Total	609.54	15				

selective holes in the membrane structure. An important point to note is that due to the selectivity of glass polymers, the presence of polyvinyl alcohol polymer in the Pebax membrane increases the selectivity(Mina Kheirtalab, Reza Abedini, 2022, 2020).

The measured CH₄ permeability of the membranes ranged from 12.77 to 35.22 (units). According to the analysis of variance (ANOVA) (Table C in the Appendix), the most suitable model to explain the relationship between the independent variables and CH₄ permeability is a modified one. The model's F-value (8.36) indicates its statistical significance. Figure D in the Appendix compares the experimental findings with the predicted values for CH4 permeability. For more detailed and precise comparisons, the normalized graph of the findings is provided in graph a of Figure D in the Appendix. Graph b in Figure D in the Appendix depicts the model's predicted values based on the actual findings. The residual values in terms of formulations are illustrated in Graph c of Figure D in the Appendix, while the residual values (deviation between the observed and predicted values) are shown in terms of the predicted values in graph d of Figure D in the Appendix. The relative error for CH4 permeability of all experimental runs fluctuated within -5.33 % and +5.33 %, as indicated on the y-axis of the graph(Sambasevam et al., 2023).

Fig. 10 illustrates the results of the CH_4 permeability test. In contrast to the effect of PVA on CO_2 permeability, increasing PVA content reduces CH_4 permeability. This can be attributed to the reduced interactions between CH_4 and PVA molecules, resulting in an increased barrier effect of PVA crystals against CH_4 molecules. The effects of MgO nanoparticles, pressure, and temperature on CH_4 permeability are similar to their effects on CO_2 permeability(Zou et al., 2023).

As the study shows that the independent variables influence CH_4 permeability. Eq. (11) exhibits the quantitative correlation between CH_4 permeability and the A to D variables derived from the regression study.

$$CH_4 Permeability = +26.21 - 8.28*A + 1.09*B + 1.93*C + 3.45*D +2.98*AC - 4.58*BC + 2.33*CD - 2.85*A^2 - 4.36*B^2$$
(11)

3.5. Molecular dynamics simulation

Comparison between experimental results and simulation data validates the reliability of experimental findings. Fig. 11 plots mean squared displacement (MSD) versus time, allowing diffusion coefficients to₂ be determined per Equation (5). This quantifies displacement of test gases from original lattice positions [ri(t) - ri(0)] during dynamic motion within the host polymer. Dividing the MSD curve slopes by $6*10^4$ calculates individual gas emission coefficients(Sateria et al., 2023). Table 3 reports diffusion coefficients for CH₄ and CO₂ through membranes featuring varied PVA loadings. The data indicates CO2 diffusion coefficients rise with increasing PVA content, whereas CH₄ values decrease. This performance trend links to membrane polarization at higher PVA proportions. As CO₂ molecule polarity matches the enriched surface environment more strongly, it preferentially permeates the material. Since selectivity relates to the diffusion coefficient ratio between gases, incorporating more PVA lowers selectivity for CH₄/CO₂ separation as a consequence of the described phenomenon.

Fig. 12 shows the evaluation of CO_2 and CH_4 diffusion coefficients obtained from molecular simulation data and gas permeability from experimental measurements at varied PVA weight percentages in dispersed polymer nanocomposites. In Fig. 12. a, the CH_4 emission coefficient from simulation decreases non-linearly with a gentle slope as PVA content rises. Fig. 12. c demonstrates experimental CH_4 permeability mirrors this trend. This occurs as higher PVA proportions enhance the material's polarity, hindering dissolution of nonpolar CH_4 . Meanwhile, Fig. 12. b illustrates the CO_2 diffusion coefficient from simulation data increases slightly with growing PVA percentage, resembling the experimental CO_2 permeability change in Fig. 12 at low pressures and temperatures. Carbon dioxide's polar vibrational nature facilitates greater penetration into the polymer matrix where PVA loading is elevated.

3.6. Optimal formulations

Further variations in gas permeability compared to each other can serve as a useful criterion for assessing the selectivity of nanocomposite membrane permeation in relation to CO_2 or CH_4 gases. Equation (12) presents the relative separation of CO_2 and CH_4 gases by the nanocomposite membrane, where P_{CO2} represents the CO_2 permeability and P_{CH4} represents the CH_4 permeability(Jasim et al., 2023).

$$Selectivity index = \frac{P_{CO_1}}{P_{CH_4}}$$
(12)

This equation reaches its highest value when P_{CH4} is the lowest and P_{CO2} is the highest. To determine the maximum value of Equation (12), a numerical method was utilized using the MATLAB software. The formulations that yielded the highest value for Equation (12) are listed in Table 4 as the optimal formulations. As the highest value of the aforementioned equation indicates the highest selectivity between the two gas types by the nanocomposite membrane, these formulations were selected as the optimal formulations. Although the practical selectivity values (α) obtained for CO₂ and CH₄ gases may differ from the selectivity index obtained through the design of experiments and molecular dynamic simulation, the trend and values of these selectivity are generally similar and close.

4. Conclusion

This study utilized a Pebax®1523 polymer matrix with polyvinyl alcohol (PVA) added at a 20 % weight ratio and magnesium oxide nanoparticles at a 10 wt% for CO₂ and CH₄ separation. The mixed matrix polymer membrane was successfully prepared via casting. The performance of the membrane was investigated at pressures of 2, 4, 6 and 8 bars and temperatures of 25, 35, 45 and 55 °C. FESEM, FTIR and XRD tests were used to evaluate the prepared membrane. FTIR results confirmed functional groups of polyether block amide, PVA, and magnesium oxide nanoparticles in the composite and nanocomposite. XRD examination showed nanoparticle addition decreased the polymer structure's peak intensity by 24° in two-theta. FESEM imaging revealed nanoparticles were more uniformly distributed with suitable polymer/ inorganic compatibility. The results showed polar/ether groups interacting with CO₂ increased carbon dioxide permeability. Nanoparticle addition enhanced CO2/CH4 permeability and selectivity versus the pure membrane, while mitigating softening. PVA presence was thought to increase crystalline points preventing gas passage. Examining pressure changes revealed permeability rose with increasing pressure from 2 to 8 bars for both gases. Variance analysis indicated the modified model best fit relationships between variables and responses. Permeability values also correlated significantly with MDS. Simulation data showed the CH₄ emission factor decreased non-linearly with gentle PVA percentage slope. Conversely, CO2 gas diffusion increased with gentle PVA percentage slope.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgment

The research mentioned in this publication was funded by a research grant from the Islamic Azad University, Shahreza Branch. The authors would like to express their gratitude to the Research Vice Chancellor of Islamic Azad University, Shahreza Branch, and their colleagues for their valuable cooperation and contributions throughout the research process.

Appendix

(See Fig. A1, Fig. B1, Fig. C1, Fig. D1, Table A1, Table B1, Table C1).

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