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# ORIGINAL ARTICLE

# Optimization study by Box-Behnken design (BBD) and mechanistic insight of $CO_2$ methanation over Ru-Fe-Ce/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst by in-situ FTIR technique



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# **KEYWORDS**

Carbon dioxide; BBD; FTIR Abstract The utilization of carbon dioxide for methanization reactions in the production of synthetic natural gas (SNG) is of increasing interest in energy-related issues. The use of CO<sub>2</sub> as a raw material in methanization reactions in the formation of SNG is of increasing concern associated with energy problems. The effect of three independent process parameters (calcination temperature, ceria loading and catalyst dosage) and their interactions in terms of conversion of CO<sub>2</sub> was considered by response surface methodology (RSM). Box-Behnken design (BBD) revealed that the optimized parameters were 1000 °C calcination temperature, 85% wt ceria loading and 10 g catalyst dosage, which resulted in 100% conversion of CO<sub>2</sub> and 93.5% of CH<sub>4</sub> formation. Reaction intermediate study by in situ FTIR showed that carboxylate species was the most active species on the catalyst surface. In-situ FTIR experiments revealed a weak CO<sub>2</sub> adsorption, that exist namely as carboxylate species over the trimetallic catalyst. As a result, dissociated hydrogen over ruthenium reacts with surface carbon, leading to \*CH, which subsequently hydrogenated to produce \*CH<sub>2</sub>, \*CH<sub>3</sub> and finally to the desired product methane. The use of in situ-FTIR study indicated that the CO<sub>2</sub> methanation mechanism does not involve CO as a reaction intermediate. The more detailed mechanism of CO<sub>2</sub> methanation pathways involved over Ru-Fe-Ce/γ-Al<sub>2</sub>O<sub>3</sub> catalyst is discussed in

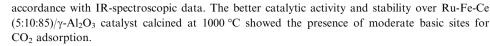
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#### 1. Introduction

The catalytic hydrogenation of CO<sub>2</sub> to CH<sub>4</sub>, known as the Sabatier reaction, as reported by Sabatier and Senderens in 1902, is a significant catalytic process (Sabatier and Senderens, 1902). The formation of CH<sub>4</sub> from CO<sub>2</sub> hydrogenation occurs in two possible pathways (a) in the process of RWGS shift, the cleavage of C—O bond results in the formation of CH<sub>x</sub> species via \*HCOH, \*H<sub>2</sub>CO<sub>2</sub> or \*H<sub>3</sub>CO intermediates, then CH<sub>x</sub> species undergo subsequent hydrogenation reactions to form CH<sub>4</sub>. Detailed studies of CO<sub>2</sub> methanation reaction by Xu et al. (2016) revealed that the formation of CH<sub>4</sub> was not seen until the appearance of formate species. They suggested that formate possibly may be a critical intermediate of the methanation reaction. Their point of view was supported by several other groups (Kustov and Tarasov, 2014; Schild et al., 1991; Wang et al., 2015). (ii) In direct cleavage of the C-O bond, the formation of CH<sub>4</sub> occurs via \*CO<sub>2</sub> dissociates and forms \*CO and \*O on various noble metal-based catalysts. \*CO undergoes a dissociation reaction to produce \*O and \*C, which is then hydrogenated to form CH<sub>4</sub>. Research conducted by Karelovic and Ruiz (2013) revealed the following statements. First, CO<sub>ads</sub> species were observed at lower temperature when RWGS did not exist. Second, CO was not detected even at 200 °C. Third, until the temperature increased to 180 °C, formate was not accompanied by COads species. Hence, they concluded that the formate species had little effect on the reaction. Similarly, the H-assisted pathway of CO dissociation over Fe and Co catalysts was proposed by Ojeda et al. (2010). Likewise, Solymosi and Pásztor (1987) conducted a spectroscopic study over supported Rh catalyst. They found that dissociation of CO on Rh may contribute to the formation of H<sub>ads</sub>. Moreover, various intermediates products were observed for the hydrogenation of CO. Thus, in both pathways, the cleavage of C—O bond in H<sub>x</sub>CO species is a very important step, and probably defines the overall selectivity of CH<sub>4</sub> in the CO<sub>2</sub> hydrogenation reaction.

In present work, the main objective of using RSM method was to obtain the best optimal conditions for experimental design. In mechanistic reactions, the interactions of  $CO_2$  at the cerium oxide and iron oxide interface that can tune the reaction mechanisms were studied. Adsorption properties of  $CO_2$  depending on the reaction temperature were studied in IR studies. In addition, the results of the FTIR studies are summarized in terms of the cleavage of the C—O bond, and the formation of the C—H bond, which gives an idea of the activation and conversion of  $CO_2$  to methane. The results are related to promote the direct route of  $CO_2$  reduction of methane.

# 2. Experimental

# 2.1. Catalyst synthesis

The Ru/Fe/Ce/γ-Al<sub>2</sub>O<sub>3</sub> catalyst was synthesized by incipient wetness impregnation method. A fixed amount of Cerium

nitrate [Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O] (Sigma-Aldrich) 5 g, requisite amount of iron nitrate [Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O] (QRëC) and ruthenium chloride [RuCl<sub>3</sub>·H<sub>2</sub>O] (Acros Organics) were dissolved in 15 mL distilled water with constant stirring for 30 min. 10 g of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support was immersed into the catalyst solution for 30 min. Next, the supported catalyst was transferred on glass wool and aged for 24 h at 90 °C. Then, it was calcined at 1000 °C for 5 h at a heating rate of 10 °C min<sup>-1</sup>.

## 2.2. Catalytic performance

The FTIR in situ method was used to study the nature of surface species during methanation of CO<sub>2</sub> using Ru/Fe/Ce/y-Al<sub>2</sub>O<sub>3</sub> catalyst. Infrared spectra (64 scans per spectrum, resolution 4 cm<sup>-1</sup>) were obtained with the help of FTIR (Brand: Nicolet Avatar 670 DGTS spectrometer) as shown in Fig. 1. For this study we used a cell of FTIR spectrometer (Brand: Nicolet Avatar 670 DGTS) equipped with KBr windows. Before the study, the catalyst was reduced in H<sub>2</sub> flow at 300 °C for 1 h, after which it was cooled down to 50 °C and background spectra were produced. Then, the reaction mixture (vol\%, CO<sub>2</sub>:  $H_2 = 1.4$ ) was fed and the spectra were obtained again. The gas hourly space velocity (GHSV) was adjusted to 636 mL g<sup>-1</sup> h<sup>-1</sup>. The spectra were recorded at intervals of 2-3 min for half an hour until it became constant. The obtained spectra were represented after background correction, and subtraction of CO<sub>2</sub> gaseous spectra.

# 2.3. Response surface methodology (RSM)

In recent years, response surface methodology (RSM) is the prevailing optimization method in use. It is a set of statistical and mathematical methods beneficial for the development, improvement, and optimization of processes. It explains the impact of independent variables, individually or in combination with each other, on the processes (Toemen et al., 2017; Rosid et al., 2018). This methodology not only analyzes the influence of independent variables, but also creates an empirical model describing the appropriate quantity of process. The experimental setup and statistical study were executed using Design-Expert software (version 7.1.6, stat-ease Inc., Minneapolis, USA). The BBD (Box-Behnken design) three-level, three-factor design was used, comprising of 15 experimental runs. In this study, three variables were included:  $(X_1)$  calcination temperature (°C), (X<sub>2</sub>) Cerium load wt% and (X<sub>3</sub>) catalyst dosage, as shown in Table 1. Each variable varied over three levels of -1, 0, +1. The generalized second-order polynomial model employed in the RSM is presented in Eq. (1):

$$Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ii} X_i^2 + \sum \beta_{ij} X_i X_j$$
 (1)

where Y represents the predicted response (i.e. initial capacity and Rate constant), whereas  $\beta_{o}$ ,  $\beta_{i}$ ,  $\beta_{ii}$ , and  $\beta_{ij}$  represent the regression coefficient for the term intercept, linear, square

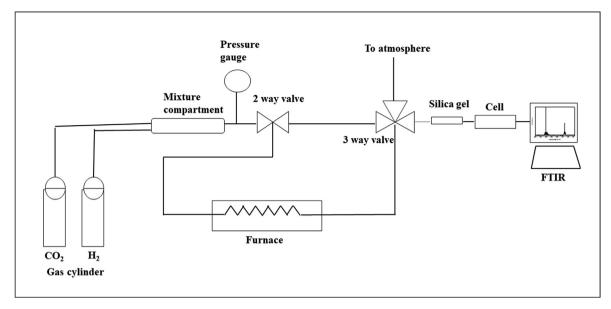


Fig. 1 Systematic diagram of the homebuilt reactor.

and interaction effects, respectively. Also,  $X_i$  and  $X_j$  are independent variables. The ANOVA table was created, and influence and regression coefficients of individual linear, quadratic and interaction terms were calculated. The values of all second-order polynomial model terms were statistically determined by calculating the F-value.

#### 3. Results and discussion

In this present study, 15 experiments were conducted under the Box-Behnken design (BBD) using Design-Expert software (version 7.1.6, Stat-Ease Inc., Minneapolis, USA) to validate the experimental results.

## 3.1. Optimization of $Ru/Fe/Ce/\gamma$ - $Al_2O_3$ by RSM method

In this study, independent variables were: (i) Calcination temperature  $^{\circ}$ C ( $X_1$ ), (ii) Ce load wt% ( $X_2$ ) and (iii) catalyst dosage (g) ( $X_3$ ), as shown in Table 1. The conditions for each process parameter varied at three levels -1, 0, +1.

According to the Box-Behnken design (BBD), experimental design and corresponding results are presented in Table 2. Based on the RSM analysis, the quadratic model for CO<sub>2</sub> conversion is shown the following Eq. (2).

$$Y = 99.35 + 3.52X_1 - 12.60X_2 + 7.62X_3 - 19.83X_1X_2 - 0.54X_1X_3 + 2.12X_2X_3 - 52.92X_1^2 + 13.36X_2^2 - 7.27X_3^2$$
 (2)

In this study, the following terms were statistically significant (i) calcination temperature  $(X_1)$ , (ii) Ce load  $(X_2)$ , (iii) catalyst dosage  $(X_3)$ , (iv) calcination temperature  $(X_1^2)$ , (v) Ce load  $(X_2^2)$ , (vi) catalyst dosage  $(X_3^2)$ , and (vii) calcination temperature - Ce load  $(X_1X_2)$ . Other model terms, including  $X_1X_3$  and  $X_2X_3$  have p-value of 0.1792 and 0.0016, which means that these terms do not have a significant impact on the model. Table 3 shows that the model p-value was lower 0.001, that indicates the high importance of the model. Moreover, Table 3 shows that the F-value is 3338.07 which indicates the high significance of the model. The probability (p-value) of most of the factors and model term is < 0.005. Thus, the model is of great importance, and all three independent variables were considered as model terms.

# 3.2. Model reliability analysis

A comparison of the actual and predicted  $CO_2$  conversion results for the  $Ru/Fe/Ce/\gamma-Al_2O_3$  catalyst is depicted in Fig. 2.

As can be seen from Fig. 2, there is a very strong convergence between the predicted values and the experimental values for  $CO_2$  conversion. It is noteworthy that Fig. 2 shows both the reliability of the variance analysis and the regression model validity. The high value of  $R^2 = 0.9998$  from Table 4, which means high accuracy and good suitability of the model.

Table 4 shows that the value of  $Pred-R^2 = 0.9983$  logically coincides with adj- $R^2 = 0.9995$ , and also difference is 0.0015, indicating the adequacy of the model applied (Huang et al., 2014). Moreover, the low value of co-efficient of variation

Table 1     Box-Behnken design experiment design and factors.					
Process variables	Code	Level Range			
		-1	0	+1	
Calcination temp. (°C)	$X_1$	900	1000	1100	
Loading of Ce (wt%)	$X_2$	80	85	90	
Catalyst dosage (g)	$X_3$	7	10	13	

No		Factor Var	Factor Variables			CO <sub>2</sub> conversion (%)	
Standard	Run	$\overline{X_1}$	$X_2$	X <sub>3</sub>	Actual	Predicated	
11	1	0	-1	+1	96.37	96.83	
10	2	0	+1	-1	56.85	56.39	
1	3	-1	-1	0	22.33	22.32	
14	4	0	0	0	100	99.35	
5	5	-1	0	-1	27.11	27.48	
2	6	+1	-1	0	69.11	69.02	
12	7	0	+1	+1	75.50	75.87	
7	8	-1	0	+1	44.25	43.80	
15	9	0	0	0	98.63	99.35	
13	10	0	0	0	99.43	99.35	
4	11	+1	+1	0	4.16	4.17	
3	12	-1	+1	0	36.68	36.77	
9	13	0	-1	-1	86.19	85.83	
8	14	+1	0	+1	50.15	49.78	
6	15	+1	0	-1	35.15	35.60	

**Table 2** Corresponding experimental design using BBD method and response values.

**Table 3** Analysis of variance (ANOVA) results for response surface second-order model for the  $CO_2$  conversion over  $Ru/Fe/Ce/\gamma$ - $Al_2O_3$  catalyst.

Source	Sum of squares	DF	Mean square	F-Value	p-value
Model	14111.58	9	1567.95	3338.07	< 0.0001 <sup>a</sup>
$X_1$	99.40	1	99.40	211.63	< 0.0001
$X_2$	1270.33	1	1270.33	2704.45	< 0.0001
$X_3$	464.67	1	464.67	989.25	< 0.0001
$X_1X_2$	1572.12	1	1572.12	3346.95	< 0.0001
$X_1X_3$	1.14	1	1.14	2.44	0.1792 <sup>b</sup>
$X_2X_3$	17.94	1	17.94	38.18	0.0016 <sup>b</sup>
$X_2X_3$ $X_1^2$ $X_2^2$ $X_3^2$	10341.55	1	10341.55	22016.48	< 0.0001
$X_2^2$	659.08	1	659.08	1403.14	< 0.0001
$X_3^2$	194.90	1	194.90	414.94	< 0.0001
Residual	2.35	5	0.47		
Lack of Fit	1.40	3	0.47	0.99	0.5391 <sup>b</sup>
Pure Error	0.95	2	0.47		
Cor Total	14113.93	14			

<sup>&</sup>lt;sup>a</sup> Significant.

(C.V.% = 1.14) reflects the fact that this model proves high reliability and good fitness.

Table 5 shows the parameters for optimization process variables to achieve maximum  $CO_2$  conversion. The main purpose to choose cerium loading as a crucial parameter in the RSM calculation due to the large capacity for storage and release of oxygen by means of redox process  $Ce^{4+} \leftrightarrow Ce^{3+}$ , it also enhanced the thermal stability of alumina support and improved the dispersion of noble metals (Kašpar et al., 1999). It is established that the mobility of surface oxygen species in  $CeO_2$  is higher in comparison with other metal oxides (Braja, 2003). Thus, 99.99% of  $CO_2$  conversion was achieved under optimal conditions of calcination temperature of 1004.16 °C at a load of Ce 84.54 wt% and catalyst dosage of 9.80 g, which were determined by RSM for this model. The RSM values were close to the experimental value (99.70%) and therefore confirmed the experimental optimization.

The 3D response surface curves were constructed for the CO<sub>2</sub> conversion model (Fig. 3). The surface plots were con-

structed as a function of two of the factors. Fig. (3a-c) shows the mutual effects of variables in the  $CO_2$  conversion. The interaction of calcination temperature and Ce load at  $CO_2$  conversion is shown in Fig. 3a. Fig. 3a shows a graph of the dependence between calcination temperature and  $CO_2$  conversion, signifying that the calcination temperature has a significant effect on  $CO_2$  conversion. As the calcination temperature rises from 900 to  $1000\,^{\circ}C$ ,  $CO_2$  conversion also increases. Meanwhile, with temperature increases from  $1000\,^{\circ}C$  to  $1100\,^{\circ}C$ ,  $CO_2$  conversion is reduced by sintering effect. Therefore, the catalyst with cerium load (85 wt%) and calcined at  $1000\,^{\circ}C$  had the highest  $CO_2$  conversion values.

Fig. 3b shows that the interactions between calcination temperature and catalyst dosage during  $CO_2$  conversion is significant. Fig. 3b shows that the maximum conversion took place with the catalyst dosage of 10 g. Fig. 3a shows that the increase in calcination temperature after 1000 °C resulted in diminution in  $CO_2$  conversion over the  $Ru/Fe/Ce/\gamma-Al_2O_3$  catalyst. Fig. 3c illustrates the effect of interaction between cerium

<sup>&</sup>lt;sup>b</sup> Not significant.

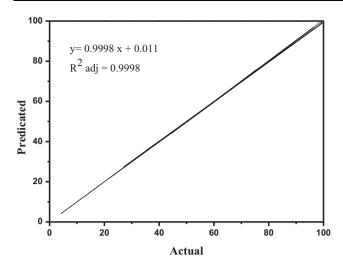


Fig. 2 Comparison of actual and predicted CO<sub>2</sub> conversion results.

Source	Result
Standard deviation	0.69
Mean	60.13
C.V. (%)	1.14
Press	24.55
$R^2$	0.9998
Adj-R <sup>2</sup>	0.9995
Pred-R <sup>2</sup>	0.9983
Adeq. precision	170.096

load and catalyst dosage on  $CO_2$  conversion. Hence, the catalyst with 85 wt% cerium load and catalyst dosage (10 g) gave the maximum conversion value of  $CO_2$  (100%) at a reaction temperature of 300 °C.

## 3.3. Methanation activity

A promising method of obtaining synthetic natural gas is the conversion of  $CO_2$  to  $CH_4$  by methanation reaction. The data of catalytic activity for methanation with FTIR over Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst at different temperatures were obtained. Before the test, the catalyst was exposed to H<sub>2</sub> atmosphere for 30 min at 300 °C. Then, it was cooled down to room temperature. The values were recorded after 20 min in steady-state conditions for each temperature. The conversion of  $CO_2$  to methane started at around 150 °C, and maximum reaction rate was around 275 °C. The maximum  $CH_4$  production was increased to 93.5% after the reaction temperature was raised

to 275 °C. Further increase in temperature, resulting in lower methane production.

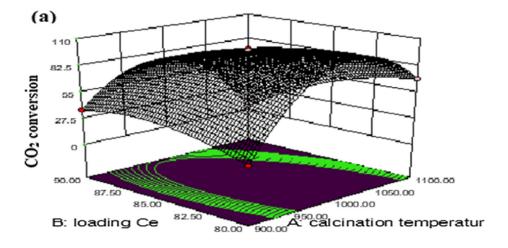
The data supporting the suggested view on CO<sub>2</sub> methanation over Ru/Fe/Ce (5:10:85)/γ-Al<sub>2</sub>O<sub>3</sub> catalyst were acquired by in situ FTIR spectroscopy. In Fig. 4, the data on CO<sub>2</sub>/H<sub>2</sub> (1:4) conversion in contact with Ru/Fe/Ce(5:10:85)/γ-Al<sub>2</sub>O<sub>3</sub> at temperatures of 50–300 °C are given. At reaction temperate of 150 °C, only 2.20% of CH<sub>4</sub> is produced over the Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, that was calcined at 1000 °C for 5 h. It is noteworthy that the peak relating to CH<sub>4</sub> at 3015.28 cm<sup>-1</sup> was not detected, as shown in Fig. 4 because it was too small to be noticed. The conversion of CO<sub>2</sub> to methane increases rapidly between temperatures at 200 and 250 °C, while it remains much more stable after reaching a catalyst reaction temperature of 275 °C. Methane selectivity (93.5%) is reduced to 89.8% after reaching the reaction temperature of 280 °C and 92.8% at 290 °C. The results show that at a reaction temperature of 275 °C, a maximum CH<sub>4</sub> production of 93.5% was observed. The selectivity towards methane was achieved 90.88%, whereas a small proportion of 9.12% was detected as a by-product. Hence, at this temperature, intensity peak of CH<sub>4</sub> was appeared and higher occurred.

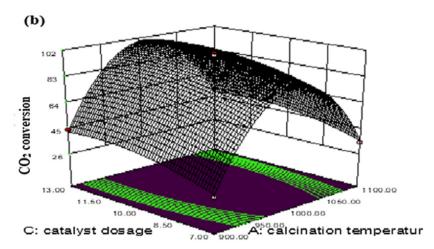
The FT-IR absorption bands assigned to the vibrational modes v(C=0) and v(C-H) species appear at 2358 cm<sup>-1</sup> and 3016 cm<sup>-1</sup> respectively. These bands were assigned to monitor the presence of CO2 and CH4. Degenerate bending modes of CO<sub>2</sub> starts at a reaction temperature of 150 °C, corresponding to a peak assigned at around 680 cm<sup>-1</sup>, and intense peak at 2351 cm<sup>-1</sup>, which corresponds to its asymmetric mode of stretching (Stevens et al., 2008). The weak feature observed between 3600 and 3800 cm<sup>-1</sup> was attributed to OH stretching mode due to surface water, which is due to the excitation of two modes (Toemen et al., 2017; Jean, 2013). Starting from the reaction temperature of 200 °C, CH<sub>4</sub> was identified in the gas phase, which is characterized by roto-vibrational bands centered at 3016 and 1305 cm<sup>-1</sup>, attributed to C-H modes of stretching and deformation modes (Nakamoto, 1997). Analysis of the region 2000-1700 cm<sup>-1</sup> showed that there was no trace of CO species.

## 3.4. Adsorption studies

Fig. 5 demonstrates the IR-spectra of  $CO_2$  on Ru/Fe/Ce (5:10:85)/ $\gamma$ - $Al_2O_3$  in  $CO_2$  methanation reactions at 50–300 °C. To further study, the adsorbed species behavior on the surface of the  $Ru/Fe/Ce(5:10:85)/\gamma$ - $Al_2O_3$  catalyst in the region between 4000 and 450 cm<sup>-1</sup>, in situ FTIR  $CO_2$  adsorption spectra at different temperatures were recorded. The postulated mechanism of  $CO_2/H_2$  methanation follows the mechanism of Langmuir Hinshelwood, which initially involves the adsorption of  $CO_2$  and  $H_2$  gases on the surface of catalyst (Langmuir, 1918). The analysis of surface species formed on  $Ru/Fe/Ce(5:10:85)/\gamma$ - $Al_2O_3$  catalyst shows absence of

Table 5     The summarized optimum conditions for RSM model.						
	Response	Goal	Lower Limit	Upper Limit	Predicated results	Experiment verified conditions
$X_1$	Calcination temperature (°C)	In range	900	1100	1004.16	1000
$X_2$	Ce load (wt%)	In range	80	90	84.54	85
$X_3$	Catalyst DOSAGE (g)	In range	7	13	9.80	10
Y	Conversion of CO <sub>2</sub> (%)	Target	90	100	99.99	99.70





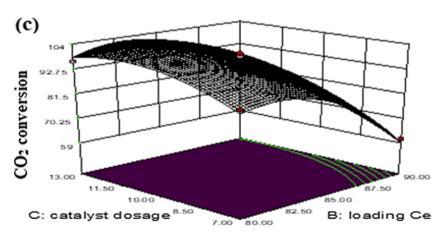


Fig. 3 RSM plots of the combined (a) calcination temperature (°C) vs Ce load (wt%), (b) calcination temperature (°C) vs catalyst dosage (g), and (c) Loading Ce (wt%) vs catalyst dosage (g) on CO<sub>2</sub> conversion.

1504 cm<sup>-1</sup> (monodentate carbonate), 1567, 1289, 1014, 856 cm<sup>-1</sup> (bidentate carbonate), 1462, 1351 cm<sup>-1</sup> (poly dentate carbonates) and 1413, 1218 cm<sup>-1</sup> (hydrogen carbonate) species (Binet et al., 1999; Yoshikawa et al., 2014). Similarly, the bands assigned to hydrogen carbonates were also absent on the surface of these samples as features at 3616, 1594, 1220

and 1060 cm<sup>-1</sup> (Daturi et al., 2000). The bands assigned to 1790, 1735, 1218–1087 cm<sup>-1</sup> (formate species) are also absent (Pan et al., 2014; Li and Domen, 1990).

The deformation band due to hydroxyl group (-OH) at (1640 cm<sup>-1</sup>) begin to form at 100 °C, it further increases in intensity to a reaction temperature of 290 °C. The adsorbed

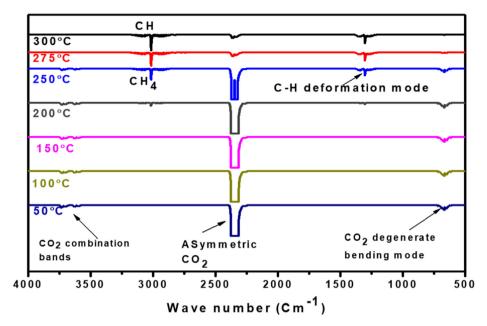


Fig. 4 FTIR spectra of gaseous phases at different reaction temperatures of  $CO_2/H_2$  methanation reaction over Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst calcined at 1000° C for 5 h.

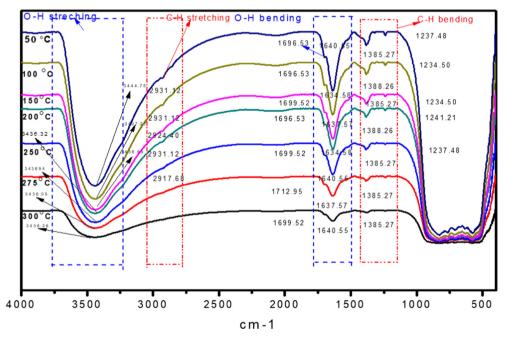


Fig. 5 FTIR spectra of adsorption species on Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> surface at different reaction temperatures calcined at 1000 °C for 5 h.

water has similar properties. The sites for the formation of surface Ce carboxylate group is available during the reaction at reaction temperature of 100 °C. This data indicates that carboxylate specie is formed on the Ru/Fe/Ce(5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst surface, when a mixture of CO<sub>2</sub>/H<sub>2</sub> (1:4) is contacted on catalyst surface during methanation reaction. The catalyst Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> showed two broad O-H regions at 3434 and 1635 cm<sup>-1</sup>, that were assigned to stretching and bending vibration of adsorbed water on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support (Muñoz-Murillo et al., 2018). The presence of OH groups

highlights the participation of OH groups in the reaction of CO<sub>2</sub> methanation (Karelovic and Ruiz, 2013). Both bands did not display significant variations throughout the reaction temperature. When the reaction temperature was 100 °C, a band appeared at 1641 cm<sup>-1</sup> (—OH) bonding with a shoulder at around 1701 cm<sup>-1</sup> corresponding to carboxylate species adsorbed on catalyst surface, as represented in Fig. 5. There is no change in the intensity of carboxylate peak. It shows that carboxylate species adsorption on the surface of very fast. The C—H stretching was started at a reaction temperature of

150 °C, at which a small amount of methane was detected at this temperature as shown in Fig. 5. When the temperature increased from 150 to 275 °C, carboxylate species were hydrogenated by dissociation of hydrogen atoms on the surface of Ru to the formation of hydrocarbon, that lead to the formation of hydrocarbons and finally methane.  $CO_2$  methanation does not take place through CO intermediate. This further proves that when the CO species was detected in the mechanistic study in the gaseous study.

# 3.5. CO<sub>2</sub> dissociative methanation reaction

The mechanism of reaction, that could consider all these observations, is presented in Fig. 6. The interface of the Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst offers multiple sites for the adsorption of intermediates reaction products. In this study, formation of CH<sub>4</sub> occurs via the direct cleavage of the C—O bond. In the direct cleavage of the C—O bond pathway, \*CO<sub>2</sub> is subjected to a dissociation reaction to form \*C and \*O, or \*C and \*CO<sub>2</sub>, followed by hydrogenation of \*C to \*HC, which is subsequently hydrogenated to produce \*CH<sub>2</sub>, \*CH<sub>3</sub> and finally the desired product CH<sub>4(g)</sub> (Weatherbee and Bartholomew, 1982).

Step 1:  $*CO_2 \rightarrow *CO_2^-$ 

Step 2:  $*CO_2^- \rightarrow *C + *O$ 

Step 3:  $*C + *H \rightarrow *CH$ 

Step 4:  $*O + *H \rightarrow *OH$ 

Step 5:  $*CH + *H \rightarrow *CH_2$ 

Step 6: \*OH + \*H  $\rightarrow$  \*H<sub>2</sub>O

Step 7: 
$${}^*CH_2 + {}^*H \rightarrow {}^*CH_3$$

Step 8: 
$$*CH_3 + *H \rightarrow CH_{4(gas)}$$

\* represents adsorbed species.

The proposed pathway for  $CO_2$  activation and methanation on Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> is shown in Fig. 6. For the methanation  $CO_2$  on Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, Ru metal sites facilitates to the dissociation of molecular  $H_2$ , and the spillover of H atoms from Ru metal sites to cerium oxide that formed carboxylate on its surface surfaces.

The CO<sub>2</sub> methanation over Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst proceeds via bending of straight chain CO<sub>2</sub> on Fe (Choe et al., 2001). Adsorption of CO<sub>2</sub> on the CeO<sub>2</sub> and Fe<sub>2</sub>O<sub>3</sub> surface and stepwise hydrogenation to methane through carboxylate intermediates by spilling hydrogen from Ru. In sum, it can be assumed that in the process of methanation CO directly dissociated to carbon (C) and O. Then, at the next stage, hydrogenation of C<sub>ad</sub> occurred. In situ IR method provide direct observation of intermediate products on the catalyst surface.

# 3.6. Stability test

The Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, calcined at 1000 °C, performed with excellent stability. The stability test graph is shown in Fig. 7.

Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, calcined at 1000 °C, was subjected to stability testing at 275 °C because of its relatively outstanding catalytic performance in CO<sub>2</sub> methanation. This is illustrated in Fig. 7, the catalyst showed the best stability for CO<sub>2</sub> conversion within 45 h, with little or no significant reduction in CO<sub>2</sub> conversion (more than 90%). The catalyst's high stability can be ascribed to its relatively moderate basicity and homogenous ruthenium distribution on the support. The

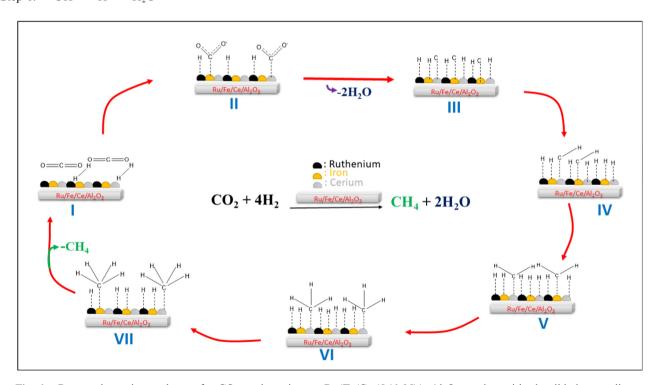


Fig. 6 Proposed reaction pathways for CO<sub>2</sub> methanation on Ru/Fe/Ce (5:10:85)/γ-Al<sub>2</sub>O<sub>3</sub> catalyst with plausible intermediates.

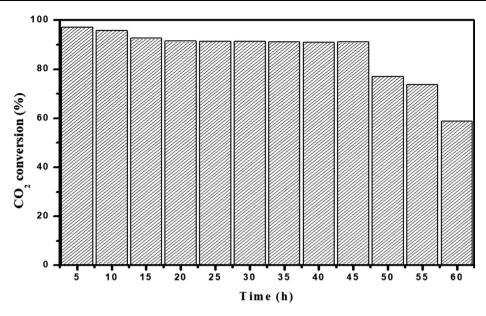


Fig. 7 Stability test result of Ru/Fe/Ce (5:10:85)/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst calcined at 1000 °C for  $CO_2$  methanation at 275 °C,  $CO_2/H_2 = 1:4$ .

Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, calcined at  $1000\,^{\circ}$ C, maintains good stability during the experimental period. The results of the catalytic study showed that the Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst, calcined at  $1000\,^{\circ}$ C, has a high potential for CO<sub>2</sub> methanation due to excellent activity and stability in reaction conditions. The better catalytic performance of Ru/Fe/Ce  $(5:10:85)/\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst could be attributed to lower iron content that led to the highest selectivity of methane formation (Kang et al., 2011), as compared to our previous work where methane formation was much lower due to high content of iron under similar reaction conditions (Ab Halim et al., 2015), and with similar content of ruthenium (Bakar et al., 2015).

# 4. Conclusion

The data obtained from in situ FTIR studies have shown that  $CO_2$  methanation occurs on Ru-Fe-Ce/ $\gamma$ -Al $_2O_3$  catalyst took place via the adsorption of  $CO_2$  on surface of ceria and iron, and then stepwise hydrogenation leads to  $CH_4$  formation through carboxylate intermediate by the hydrogen spilled over from Ru surface.

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