

ORIGINAL ARTICLE

King Saud University

Arabian Journal of Chemistry

www.ksu.edu.sa







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Received 11 April 2023; accepted 7 August 2023 Available online 22 August 2023

KEYWORDS

Supercritical carbon dioxide; Solubility; Buprenorphine hydrochloride; Sodeifian model; Peng-Robinson equation of state **Abstract** Nowadays, supercritical fluids (SCFs) technologies present a processing option for obtaining new products with noteworthy characteristics. Access to reliable solubility data of pharmaceutical compounds in SCFs is considered as the first step for recrystallizing, separating, and producing nano particles via processes based on this type of technique. In this study, high-pressure solubility of buprenorphine hydrochloride, a strong pain reliever, in supercritical carbon dioxide (scCO₂) was measured at temperature and pressure conditions of 308–338 K and 120–270 bar, for the first time. The minimum and maximum solubility values, in terms of equilibrium mole fractions, were found to be 0.131×10^{-4} (at 338 K and 120 bar) and 4.752×10^{-4} (at 338 K and 270 bar), respectively. Thereafter, the obtained data were correlated using two different approaches, namely Peng-Robinson (PR) equation of state (EoS) and a set of semi-empirical models. Results from applying statistical criteria indicated that Jouyban and Sodeifian models are suitable choices for predicting solubility data. Furthermore, using the obtained correlation results, the total and vaporization enthalpies of buprenorphine hydrochloride dissolution in scCO₂ were estimated to be 65.59 and 85.60 kJ/mole, respectively.

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https://doi.org/10.1016/j.arabjc.2023.105196

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1. Introduction

Buprenorphine hydrochloride is a semi-synthetic opiate and in a class of medications called narcotic analgesics. By exhibiting a unique functionality related to its concurrent agonist and antagonist activities, buprenorphine can block pain signals through binding either to the specific cellular receptors or on the surface of the nerve cells at different organs of the body. Therefore, it is capable of relieving moderate to severe pain from different origins, (e.g., surgical operation, injuries, and cancer (Heel et al., 1979) with an analgesic potency greater than that of morphine. Nowadays, they are commonly applied for the treatment of opioid dependency such as heroin addiction. Buprenorphine carries a complex-structure molecule with a lipophilic nature. The structural formula for buprenorphine is given in Fig. 1 (Johnson et al., 2005).

Although different delivery formulations for buprenorphine have been presented, oral bioavailability of this medicine, in the form of both syrup and tablet, was reported to be low (Poliwoda et al., 2022). It means that a high dose of the medicine is required to obtain the planned pharmacological effects, especially for the treatment of opioid dependency for which a much more doses are needed. This associated issue not only with buprenorphine but with a great deal of lipophilic medicines is one of the most important problems facing pharmaceutical industries. However, a number a solutions have been investigated to tackle the problem, one of which is minimizing the size of buprenorphine particles to micro and nano scale (Desai et al., 2012). Reduction of the particle size of the solids through conventional techniques such as recrystallization and spray drying often forces some disadvantages including high energy and organic solvent consumption, environmental pollution and thermal degradation of the products. In recent years, several green and efficient processes based on SCFs technologies such as rapid expansion of supercritical solutions (RESS (Türk, 2022)) and supercritical anti-solvent (SAS (Reverchon et al., 2007)) have attracted attentions due to their beneficial advantages (De Marco, 2022), which cause them to surpass conventional technologies through bringing desirable particle size distribution, reducing the possibly side effects of the drugs, and effectively improving the bioavailability and bioactivity of the medical compounds. To develop and commercialize these pharmaceutical processes, reliable experimental data on the solubility behavior of solid drugs at different conditions of temperature and pressure of the supercritical medium along with phase transitions of the system are of high value. While access to these solubility data through experimental performances are often laborious and time consuming, the use of mathematical approaches such as thermodynamic equations of state (EoSs), empirical and semi-empirical models and other predictive methods on the basis of artificial intelligence (AI) are greatly helpful to researchers. In this regard, selection of a well-established way with an acceptable accuracy is crucial. Frequently used cubic EoSs for CO₂ containing systems include Peng-Robinson (Araújo and Meireles, 2000; Lopez-Echeverry et al., 2017; Notej et al., 2023; Sodeifian et al., 2023) and modified Redlich-Kwong (Sako et al., 1988; Valderrama and Silva, 2003; Madras, 2004; Heidaryan and Jarrahian, 2013) EoSs with different mixing rules such as Wong-Sandler (WS), Orbey-Sandler (OS), van der Waals types 1 or 2 (vdW1 and vdW2, respectively), Huron-Vidal (HV), Kwak-Mansoori (KM), and covolume dependent (CVD) (Shimoyama et al., 2008; Esmaeilzadeh et al., 2009; Mansoori and Ely, 1985; Kwak and Mansoori, 1986; Lashkarbolooki et al., 2011; Sodeifian et al., 2023). On the other side, several semi-empirical density based models were proposed in recent decades for solid-fluid equilibrium including Adachi-Lu (Adachi and Lu, 1983); Kumar-Johnston (Kumar and Johnston, 1988); del Valle-Aguilera (Del Valle and Aguilera, 1988); Chrastil (Chrastil, 1982), Bartle (Bartle et al., 1991), Mendez-Santiago-Teja (Méndez-Santiago and Teja, 1999); Keshmiri (Keshmiri et al., 2014); Bian (Bian et al., 2016); Khansary (Khansary et al., 2015), and Alwi-Garlapati (Alwi and Garlapati, 2021). However, correlation process of an EoS with experimental data is more complicated than that of semi-empirical models. Because the former requires many thermodynamic properties of pure solid solute such as critical tem-



Fig. 1 Chemical structure of buprenorphine hydrochloride.

perature and pressure as well as Pitzer's acentric factor, while the latter is independent of these properties and has been developed only by involving equilibrium conditions and density of the system. General form and the number of adjustable parameters are the main differences among semi-empirical models. These adjustable parameters differ from one solute to another and are usually determined by least square curve fitting with experimental data. It seems that density based semi-empirical models with more adjustable parameters show better accuracy for correlating the experimental data. Application of different machine learning-based models such as Kernel Ridge Regression (KRR), Random forest (RF), and Multilayer Perceptron (MLP) are the other subjects of recently published papers that have reported to successfully predict and optimize the solid solutes solubility especially pharmaceutical compounds in the SCFs (Alzhrani et al., 2022; Najmi at el., 2022; Nateghi et al., 2023; Rezaei et al., 2022; Tianhao et al., 2022). Lower sensitivity to incomplete or noisy experimental data, reduced time consumption, and better fitting with solubility points of nonlinear behavior have caused the machine learning- based models to find more popularity among researchers (Cao et al., 2021; Waskita et al., 2023).

Considering the critical constants of the compounds available in the literature (Sapkale et al., 2010) to be employed in the SCFs technologies, ethane and ethylene would be found appropriate at first. But it should be noted that several factors such as flammability and explosive properties can restrict their usage. Being non-flammable, non-toxic, and nonexpensive as well as involving other favorable properties (Nikolai et al., 2019), supercritical carbon dioxide (scCO₂) has been known as the most applied agent in the different fields of research and development, e.g., material processing (Eckert et al., 1996; Zhang et al., 2014), oil and gas industry (Pavlova et al., 2022), catalyst regeneration (Vradman et al., 2001; Ghadirinejad et al., 2021), extraction from natural substrates (Liza et al., 2010; Sodeifian et al., 2017; Sodeifian and Sajadian, 2017; Tyśkiewicz et al., 2018; Hossein Zadeh et al., 2023), fabrication of polymer foams and hydrogels (Daneshyan and Sodeifian, 2022a,b; Kong at el., 2016; Liang and Wang, 2000; Tsioptsias et al., 2011), nanoparticle formation (Byrappa et al., 2008; Erkey, 2009; Ardestani et al., 2020; Franco and De Marco, 2021; Sodeifian et al., 2022), power generation (Crespi et al., 2017; White et al., 2021), and chromatographic analysis (Bernal et al., 2013; Desfontaine et al., 2015).

The focus of this research is to identify the solubility behavior of buprenorphine hydrochloride in $scCO_2$ and to evaluate the correlating ability of Peng-Robinson (PR) EoS and a set of well-known density based models. For this purpose, the equilibrium solubility of buprenorphine hydrochloride in $scCO_2$ was measured at temperatures of 308–338 K and pressures of 120–270 bar. Thereafter, the obtained experimental data were applied with the following approaches:

1) PR EoS with two different mixing rules, namely van der Waals type 2 (vdW2) and covolume dependent (CVD),

2) Eight semi-empirical models, namely Chrastil, Madras, Bartle, Jouyban, Bian, Wang, Belghait and Sodeifian models.

To determine the capability of each model for describing the solubility of buprenorphine hydrochloride in scCO₂, some statistical criteria including average absolute relative deviation (*AARD*%), adjusted correlation coefficient (R_{adj}), and *F*-test were applied.

2. Experiment

2.1. Materials

Buprenorphine hydrochloride in the form of crystalline white powder, with the purity exceeding 99% was purchased from Temad CO. (Karaj, Iran). More information on the physicochemical properties of buprenorphine hydrochloride is listed in Table 1. Carbon dioxide (CO₂), compressed in the storage cylinder, with a purity of 99% was supplied by Fadak Company (Kashan, Iran). An Analytical reagent grade of methanol with the minimum purity of 99.5%, produced by Merck (Darmstadt, Germany), was selected as the collecting solvent for buprenorphine hydrochloride after the solubility process.

2.2. Apparatus and experimental procedure

Fig. 2 gives a general view on the experimental process utilized to measure the solubility of buprenorphine hydrochloride in scCO₂. As can be seen, CO₂ storage cylinder, refrigerator, reciprocating pump, oven, temperature and pressure controlling devices, equilibrium cell, and sample collector make the main parts of the process. Directing from storage cylinder to the refrigerator, after passing a molecular sieve filter with a pore size of 1 µm, gaseous CO₂ got liquefied and ready for pumping. Installed after refrigerator, the reciprocating pump (Haskel pump, MSHP-110) provided the desired pressure of supercritical state for CO₂. Applying a pressure gauge (WIKA, Germany), the pressure of scCO₂ was monitored at an uncertainty of 1 bar. Furthermore, a precise oven (Froilabo AE-60, France) played the role of keeping and controlling the planned temperature of solubility tests at an uncertainty of 0.1 K, through a digital display showing regulated and actual temperature values. Each experiment was started by introducing prepared scCO₂ into the solubility cell containing uniformly mixed powder and glass beads. By fixing filter plates on the both ends of the equilibrium cell, undissolved particles were prevented from running out. After passing the equilibration time, set to 60 min, a given volume of saturated fluid was discharged through the sampling loop into a collection vial preloaded with 4 ml methanol. Then, by introducing 1 ml methanol into the rinse tube, precipitated particles in the sampling tube were also discharged.

The concentration value of buprenorphine in each collection vial was determined using an established calibration curve obtained from concentration analyzing the solutions on an UV–Vis spectrophotometer (Cintra-101) at the maximum wavelength (λ_{max}) of 285.5 nm (see Table 1). For this purpose, buprenorphine solutions along with a set of standard ones were loaded on the quartz cells of the spectrophotometer setup. Using the obtained absorbance results, the equilibrium mole fraction (y_2) and solubility (S_2 , in terms of gram per liter) values of buprenorphine in scCO₂, corresponding to different operating conditions, were calculated as follows:

$$y_2 = \frac{n_2}{n_1 + n_2} \tag{1}$$

$$n_1 = \frac{\rho_1 \times V_l}{M_1} \tag{2}$$

$$n_2 = \frac{C_2 \times V_S}{M_2} \tag{3}$$

$$S_2 = \frac{C_2 \times V_S}{V_l} \tag{4}$$

Where, *n* and *M* are the number of moles and molecular mass of the components (see Table 1), respectively. The system was assumed to be binary, i.e., including carbon dioxide (denoted by subscript 1) and buprenorphine hydrochloride (denoted by subscript 2). ρ_1 represents density of CO₂ at the corresponding temperature and pressure of each test. V_s and V_l are the volumes of the collected solution (5×10^{-3} L) and sampling loop (600×10^{-6} L), respectively. C_2 as the concentration of buprenorphine (in terms of gram per liter) corresponding to each test, was obtained from the calibration curve. To define a direct relationship between the equilibrium solubility and mole fraction of buprenorphine hydrochloride in scCO₂, Eq. (4) can be rewritten in the following form:

$$S_2 = \frac{\rho_1 \times M_2}{M_1} \times \frac{y_2}{1 - y_2}$$
(5)

Sodeifian and coworkers have utilized repeatedly this apparatus for different scCO₂ based processes associated with medical compounds such as solubility measurements of hydro- and lipophilic drugs (Sodeifian et al., 2018; Sodeifian et al., 2023; Abadian et al., 2023; Sodeifian et al., 2023), impregnation of solid medicines into polymer films (Ameri et al., 2020; Fathi et al., 2022), production of medical nanoparticles via various techniques including gas anti-solvent (GAS (Sodeifian et al., 2022)), rapid expansion of supercritical solution with and without solid co-solvent (RESS-SC (Sodeifian and Sajadian, 2018) and RESS (Sodeifian et al., 2019), respectively), rapid expansion of supercritical solution into aqueous solution (RESSAS (Sodeifian et al., 2019), and ultrasonic assisted rapid expansion of a supercritical solution into a liquid solvent (US-RESOLV (Sodeifian and Sajadian, 2019; Razmimanesh et al., 2021)). Therefore, further details about the apparatus are available in their published papers.

Table 1 Ph	rysicochemical	properties	of the	materials	utilized	in	this	stud	y
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Compound	Expanded formula	CAS Number	Molar mass, M (g/mole)	Peak wavelength at ultraviolet spectrum, λ_{max} (nm)	Purity
Buprenorphine HCl	C ₂₉ H ₄₂ ClNO ₄	53152-21-9	504.10	285.5	≥ 99%
Carbon dioxide	CO_2	124-38-9	44.01	_	99%
Methanol	CH ₃ OH	67–56-1	32.04	207	$\geq 95\%$

Table 2Thermodynamic cubic EoS investigated in this work.
$$PR_{EoS}$$
 $P = \frac{RT}{\bar{V}-b} - \frac{a}{\bar{V}^2 + 2b\bar{V}-b^2}$ $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ $\alpha b_i = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$ $\alpha (T_{r,i}, \omega_i) = (1 + k(1 - T_{r,i}^{\frac{1}{2}}))^2$ $k = 0.37464 + 1.54226\omega_i - 0.26992\omega_i^2$

3. Mathematical approaches

3.1. Equations of state (EoSs)

Considering thermodynamics principles (Prausnitz et al., 1998), equilibrium mole fraction of a solid solute in a high pressurized fluid can be calculated by equating the fugacity values of the considered component in two phases, as presented below:

$$f_i^{solid} = f_i^{fluid}(P, T, y_i) \tag{6}$$

Where f_i^{solid} and f_i^{fluid} are fugacity values of component i in the solid and fluid phases, respectively. Each side of Eq. (6) can be replaced by the following relationships:

$$f_i^{solid} = P_i^* \varphi_i^* \exp \frac{1}{RT} \int_{P_i^*}^P v_i^{solid} dP$$
⁽⁷⁾

$$f_i^{fluid}(P, T, y_i) = y_i P_T \varphi_i^{fluid}$$
(8)

Where y_i and P_i^* represent equilibrium mole fraction and partial pressure of the solute in the mixture at equilibrium conditions. *R* represents universal constant of ideal gas. By involving assumptions below, the final form of Eq. (6) can be simplified to Eq. (9):

1) As mentioned above, the system is composed of two components, i.e., $scCO_2$ (denoted by subscript 1) and buprenorphine hydrochloride (denoted by subscript 2).

2) Solid phase is thoroughly pure, composed of component 2.

3) Carbon dioxide is insoluble in the solid phase.

4) Solid molar volume (V_2^{-solid}) is persistently constant, independent of the fluid pressure.

5) Equilibrium pressure of the system (P) is much higher than solute's vapor pressure (P_2^*) .

6) Fugacity coefficient of the solute at equilibrium (φ_i^*) equals 1, because of its negligible vapor pressure (P_2^*) .

$$y_2 = \frac{P_2^*}{P\varphi_2^{fluid}} exp\left(\frac{P \ v_2^{\ solid}}{RT}\right)$$
(9)



Fig. 2 Schematic representation of the experimental setup utilized in this study.

As can be seen, equilibrium solubility of buprenorphine, in terms of mole fraction, depends on its physical properties, i.e., vapor pressure, fugacity coefficient in fluid phase (φ_2^{fluid}), and solid molar volume (v_2^{solid}) at the equilibrium temperature and pressure of the system. With respect to this fact the required data to solve Eq. (9) for buprenorphine have not yet been reported, the group contribution methods were followed to estimate the values. For this purpose, the methods proposed by Lee-Kesler (Lee and Kesler, 1975) and Fedors (Fedors, 1974) were used in this study to estimate values of P_2^* and v_2^{solid} , respectively. φ_2^{fluid} was also computed by the relationship below, applying Peng-Robinson (PR) EoS (Peng and Robinson, 1976), with the detailed presentation in Table 2. In Eq. (10), V and Z are the volume and compressibility factor of the system.

$$RTln\varphi_2^{fluid} = -RTlnZ + \int_{V}^{\infty} \left[\left(\frac{\partial P}{\partial n_2} \right)_{T,V,n_1} - \frac{RT}{V} \right] dV$$
(10)

In PR EoS (Table 2), v is molar volume of the system and the subscripts c and r indicate the critical and reduced values of temperature and pressure, respectively. a_i and b_i represent energy (or attractive) and volume (or repulsive) terms of the fluid phase at the thermodynamic equilibrium. In the case of single-component systems, they are calculated from the mentioned relationships, using critical properties (T_c , P_c) and the Pitzer's acentric factor of the considered compound (see Table 2). Whereas, a suitable mixing rule should be inserted for multi-components systems. For the binary system investigated in the present work twin parametric van der Waals (vdW2) and covolume dependent (CVD) mixing rules, presented in Table 3 were applied (Esmaeilzadeh et al., 2009; Mansoori and Ely, 1985).

In Table 3, y and x represent the mole fractions of each component in vdW2 and CVD mixing rules, respectively. Subscript m denotes mixture for the respective parameters. a_{ii} and a_{jj} are the energy terms of the pure components i and j, respectively. The binary interaction parameters in vdW2 (i.e., k_{ij} and l_{ij}) and CVD (i.e., M_{ij}) mixing rules are determined by optimization of differences between experimental values and those calculated from the corresponding equation of state, assuming that $M_{ij} = M_{ji}$ and $M_{ii} = M_{jj} = 1$ (Mukhopadhyay and Rao, 1993).

3.2. Density based models

Empirical and semi-empirical models are other theoretical approaches to predict solid solute solubility in $scCO_2$, with or without co-solvents, over a wide range of temperature and

Table 3 Mixing rules examined in this work.

Mixing rule	Parameter a	Parameter b
vdW2	$a_m = \sum_i \sum_j y_i y_j a_{ij}$	$b_m = \sum_i \sum_j y_i y_j b_{ij}$
	$a_{ij} = \sqrt{a_{ii}a_{jj}}(1-k_{ij})$	$b_{ij} = \frac{b_i + b_j}{2} (1 - l_{ij})$
CVD	$a_m = \sum \sum x_i x_j a_{ij} \left(\frac{b_m}{b_{ij}}\right)^{M_{ij}}$	$b_m = \sum x_i b_i$
	$a_{ij} = \sqrt{a_{ii}a_{jj}}$	$b_{ij} = \sqrt{b_{ii}b_{jj}}$

pressure. These models can be divided into density-based, association and complex models. Because of limited information on the thermodynamic properties of different solid solutes, semi-empirical models are always regarded as an acceptable alternative to thermodynamic EoSs. In this study, eight semi-empirical density-based models, presented in Table 4, were used to correlate the experimental solubility of buprenorphine hydrochloride in scCO₂.

In the above mentioned models (see Table 4), S_i and y_i are the equilibrium solubility and mole fraction of the solid solute in the fluid phase, respectively. T and P represent temperature and pressure of the system in Kelvin and bar, respectively. The subscript *ref* in Bartle model indicates the reference values of the corresponding parameters, i.e., P_{ref} and ρ_{ref} are reference pressure of the system and reference density of scCO₂ which were set to 1 bar and 700 kg/m³, respectively. a_0 - a_7 are also the adjustable parameters for each model.

3.3. Statistical criteria

Among numerous statistical techniques available to assess the correlating ability of the previously mentioned approaches, based on comparing solubility values predicted by each one with those obtained experimentally, average absolute relative deviation percent (AARD%) along with two complementary criteria, including adjusted correlation coefficient (R_{adj}) and *F*-test was selected in this study. In order to compare the ability of two models, each one includes different numbers of parameters, the modified form of AARD% as Eq. (11) is often used (Jouyban et al., 2002; Sodeifian et al., 2020).

$$AARD\% = \frac{100}{N-z} \sum_{i=1}^{N_i} \frac{|y_i^{\ cal} - y_i^{\ exp}|}{y_i^{\ exp}}$$
(11)

Where N and z are the number of data points and adjustable parameters in each model, respectively. y_i^{cal} and y_i^{exp} represent calculated and experimental equilibrium mole fraction of buprenorphine hydrochloride in fluid phase, respectively, and subscript *i* indicates the number of experimental run.

Adjusted correlation coefficient (R_{adj}) and F - value are also utilized to assess how well a function can be fitted to the experimental data. These parameters are mathematically defined as below (Jouyban et al., 2002; Sodeifian et al., 2018):

$$R_{adj} = \sqrt{\left| R^2 - \left(\frac{Q(1-R^2)}{N-Q-1}\right) \right|}$$
(12)

$$R^2 = 1 - \frac{SS_E}{SS_T} \tag{13}$$

Where, Q (in Eq. (12)) is the number of independent variables in the model. The correlation coefficient (R^2) was also obtained using the error sum of squares (SS_E) and total sum of squares (SS_T).

$$F - value = \frac{\frac{SS_R}{2}}{\frac{SS_E}{N-Q-1}} = \frac{MS_R}{MS_E}$$
(14)

Where, SS_R is the regressive sum of squares of each investigated model. MS_R and MS_E are also regressive and error mean of squares, respectively (Montgomery, 2017).

 Table 4
 Semi-empirical models investigated in this study.

Name	Relationship	References
Chrastil	$lnS_i = a_0 ln_{CO_2} + \frac{a_1}{T} + a_2$	(Chrastil, 1982)
Garlapati-Madras	$lny_i = a_0 + (a_1 + a_2)ln + \frac{a_3}{T} + a_4ln(T)$	(Garlapati and Madras, 2010)
Bartle	$ln(y_i P/P_{ref}) = a_0 + a_1(CO_2 - ref) + \frac{a_2}{T}$	(Bartle et al., 1991)
Bian	$lny_i = a_0 + \frac{a_1}{T} + \frac{a_2}{T} + (a_3 + a_4)ln$	(Bian et al., 2016)
Jouyban	$lny_i = a_0 + a_1 + a_2P^2 + a_3PT + \frac{a_4T}{P} + a_5ln$	(Jouyban et al., 2002)
Wang	$lnS_i = (a_0 + \frac{a_1}{2})ln + a_2 + a_3$	(Wang et al., 2016)
Belghait	$lny_i = a_0 + a_1 + a_2^2 + a_3T + a_4T + a_5T^2 + a_6ln + \frac{a_7}{T}$	(Belghait et al., 2018)
Sodeifian	$lny_i = a_0 + a_1 \frac{P^2}{T} + a_2 ln(T) + a_3(ln) + a_4 P lnT + a_5 \frac{ln}{T}$	(Sodeifian et al., 2019)

4. Results and discussion

4.1. Experimental data

To ensure that the methodology is reliable and standard, the apparatus and procedure were previously validated by examining the solubility of α -Tocopherol and Naphthalene at different temperatures and pressures and comparing the acquired results with the available ones in the literature (Sodeifian et al., 2018).

Following the above mentioned experimental procedure, solubility of buprenorphine hydrochloride in $scCO_2$ was determined at temperatures ranging from 308 to 338 and pressures within 120–270 bar. To improve the accuracy of the measurements, each run was performed three times. So each reported datum is the average value of three independent experimental data. The obtained results including equilibrium mole fraction

and solubility $(y_2$ and S_2 , respectively), calculated using the Eqs. (1-4), are summarized in Table 5. As can be seen, the minimum and maximum values, in terms of equilibrium mole fraction, were both at temperature of 338 K, with the values of 0.131×10^{-4} and 4.752×10^{-4} , respectively. Depicted on Fig. 3, are the obtained equilibrium mole factions applied versus CO₂ density values, at the corresponding temperature and pressure of the system. For this purpose, the required density (ρ) of scCO₂ associated with each point was obtained from National Institute of Science and Technology (NIST) data base (Chemistry WebBook, 2023). As shown, there is an increase in equilibrium mole fraction values when CO₂ density increases. Besides, Fig. 4 shows that solubility isotherms have a growing trend along the pressure of the system. In fact, transportation of buprenorphine particles into the fluid phase improves with increasing density followed by increasing solvating power of carbon dioxide under higher pressures (Sodeifian

Temperature, T (K)	Pressure, P (bar)	Density of scCO ₂ ¹ , ρ (kg/ lit)	Mole fraction, $y_2 \times 10^4$	Equilibrium solubility ² , S (g/ L)	Experimental standard deviation ³ , $S(y_i) \times 10^4$	Expanded uncertainty of mole fraction ⁴ , U \times 10 ⁴
308.1	120	769	0.691	1.076	0.011	0.037
	150	817	0.752	1.233	0.014	0.044
	180	849	0.811	1.393	0.021	0.054
	210	875	0.972	1.720	0.041	0.092
	240	896	1.120	2.029	0.051	0.113
	270	914	2.092	3.838	0.062	0.153
318.1	120	661	0.513	0.680	0.012	0.032
	150	744	0.631	0.950	0.022	0.051
	180	791	0.970	1.546	0.041	0.093
	210	824	1.233	2.050	0.051	0.114
	240	851	1.421	2.430	0.072	0.153
	270	872	2.440	4.279	0.063	0.181
328.1	120	509	0.322	0.334	0.015	0.024
	150	656	0.451	0.597	0.011	0.030
	180	725	1.190	1.745	0.051	0.115
	210	769	1.423	2.199	0.019	0.073
	240	802	2.431	3.918	0.121	0.264
	270	829	3.872	6.447	0.183	0.404
338.1	120	388	0.131	0.107	0.004	0.010
	150	557	0.202	0.232	0.008	0.018
	180	652	1.491	1.961	0.061	0.141
	210	710	1.724	2.454	0.058	0.139
	240	751	2.851	4.310	0.041	0.150
	270	783	4.752	7.483	0.065	0.246



Fig. 3 Solubility of buprenorphine hydrochloride vs. scCO₂ density at different temperatures.



Fig. 4 Solubility of buprenorphine hydrochloride vs. pressure at different temperatures.

Table 6 Approximate values of physicochemical properties of buprenorphine hydrochloride.								
Boiling	Critical	Critical	Pitzer's Acentric	Solid molar	Vapor	pressure,	$P^*(bar)$	
point, $T_b(K)$	temperature, $T_c(K)$	pressure, $P_c(bar)$	factor, ω	volume, $v^{solid}(\frac{cm^3}{mol})$	308 K	318 K	328 K	338 K
779	947.39	10.025	1.041	370.40	0.095	0.513	2.450	10.520

and Usefi, 2023). Furthermore, it can be seen that the isotherms intersect at the pressure region of 150–180 bar, leading to appearance of the crossover pressure point. This phenomenon is often attributed to the situation at which the powers of two competing factors, namely solid's vapor pressure and carbon dioxide density, are being equal. The effect of temperature on solid solute solubility is contradictory with an isobaric change before and after the crossover point, shown in Fig. 4. In fact, the antagonistic behavior of temperature indicates that the prevailing factor on solubility at 120–150 bar is CO_2 density reduction, whereas the progressive behavior of temperature at 180–270 bar shows that enhancement of solute's vapor pressure prevails (Brunner, 2005). The crossover phenomenon and dualistic effect of temperature have been frequently observed in the literature for the solubility of different compounds in scCO₂ (Adenekan and Hutton-Prager, 2020; Araus, 2011; dos Santos, 2019; Sajadian, 2023; Sodeifian et al., 2019a,b; Yang, 2020).

- 1. CO₂ density at different conditions of temperature and pressure were obtained from National Institute of Standards and Technology (NIST) database (Chemistry WebBook, 2023).
- 2. The equilibrium solubility value can also be calculated directly from equilibrium mole fraction, using Eq. (5).
- 3. Experimental standard deviation was determined from $S(y_i) = \sqrt{\sum_i (y_j \bar{y})/n 1}.$
- 4. Expanded uncertainty was calculated by $U = k.u_{combined}$ and the relative combined standard uncertainty $(u_{combined})$ was obtained from $u_{comb}/\bar{y} = \sqrt{\sum_i (P_i.u_i(x_i)/x_i)^2}$. Standard uncertainty values for temperature u(T) and pressure u(P) were ± 0.1 K and ± 1 bar, respectively. The value of the coverage factor (k) was set to 2 on the basis confidence level of approximately 95 percent.

	Temperature	M_{ij}	k_{ij}	l _{ij}	R_{adj}	F-value	AARD%
PR + vdW2	308	_	0.263	0.313	0.285	0.812	16.533
	318		0.257	0.303	0.654	2.869	15.839
	328		0.264	0.329	0.921	15.022	22.495
	338		0.279	0.363	0.961	31.298	24.388
PR + CVD	308	0.705			0.461	1.673	32.732
	318	0.696			0.754	4.287	38.015
	328	0.675			0.950	24.238	35.329
	338	0.657			0.932	17.540	40.165



Fig. 5 Comparison of experimental data (point) and calculated (line) solubility isotherms for buprenorphine hydrochloride in $scCO_2$ based on PR EoS with vdW2 (a, b) and CVD (c, d) mixing rules.



Fig. 5 (continued)

Table 8 Correlation results of buprenorphine hydrochloride solubility with semi-empirical models.

	Chrastil	Madras	Bartle	Jouyban	Bian	Wang	Belghait	Sodeifian
a_0	9.329	56.948	27.035	17.443	-4.474	22.96	-140.046	-79.103
a_1	-7.889×10^{3}	0.417	-1.029×10^{4}	-34.959	0.019	-4.401×10^{4}	-0.247	4.399
a_2	-37.506	0.002	0.014	-2.20×10^{-5}	2.782×10^{4}	-7.068	5.798×10^{-5}	8.889
<i>a</i> ₃	—	-9.428×10^{3}	—	9.764×10^{-5}	-42.990	-135.203	3.278×10^{-4}	0.002
a_4		-4.024	—	1.610	-62.520	—	-0.528	-0.122
a_5		—	—	28.779	—	—	5.393×10^{-4}	-2.179×10^{3}
<i>a</i> ₆		—	—		—	—	48.156	—
a_7		—	—		—	—	-0.501	—
AARD%	25.41	21.39	24.85	17.16	19.66	23.41	20.03	18.14
R _{adj}	0.952	0.962	0.959	0.989	0.985	0.959	0.972	0.986
F-value	76.58	81.20	77.79	89.21	83.98	78.54	82.91	85.88

4.2. Results from correlation of solubility data

According to what was mentioned above, two approaches were followed to correlate the experimental values as the second step of the recent investigation, including PengRobinson (PR) EoS and a set of semi-empirical models. Thereafter, to evaluate prediction capability, not only the correlation results of each one were determined using statistical criteria but their predicted isotherms were also brought on the diagram to be visually compared with the experimental data points.



Fig. 6 Experimental data (points) and regressed solubility isotherms from investigated density based models (lines) for buprenorphine hydrochloride- $scCO_2$ system.

4.2.1. Correlation results applying Peng-Robinson equation of state

Following theoretical procedure mentioned in section 3.1, fugacity coefficient followed by equilibrium mole fraction of buprenorphine hydrochloride was calculated, applying Peng-

Robinson EoS with two different mixing rules (PR + vdW2 and PR + CVD) at the corresponding conditions of each experimental run. The required physicochemical properties of buprenorphine hydrochloride including boiling point (T_b), critical values (T_c , P_c), and Pitzer's acentric factor (ω), presented



Fig. 6 (continued)

in Table 6, were estimated using Marrero-Pardillo (Marrero-Morejón and Pardillo-Fontdevila, 1999); Wilson-Japerson atomic contribution and Ambrose-Walton correspondingstate methods (Poling et al., 2001), respectively. Acentric factor and critical values of carbon dioxide were also set to 0.274, 304.2 K, and 73.8 bar.

Adjustable parameters of the mixing rules, i.e., k_{ij} , l_{ij} in vdW2 and M_{ij} in CVD were calculated at the optimum level by minimizing the contrast between calculated and experimental solubility data (Haghtalab and Sodeifian, 2002). Results of correlating Peng-Robinson EoS with experimental data are presented both in Table 7 and in Fig. 5. As can be seen in



Fig. 6 (continued)

Table 7, deviations between predicted solubility and experimental values grow for both equations when temperature increases. Furthermore, the deviation obtained by PR + CVD at 308 K is observed to be about two times that of PR + vdW2 and even more at 318 K. However, PR + CVD shows more suitable correlation results compared to PR + vdW2 at 308, 318, and 328 K, in terms of *F*-value and R_{adj} . But at 338 K, it can clearly be concluded that PR + vdW2 is superior to PR + CVD for thermodynamic modeling of the investigated system.

Fig. 5 shows the correlated solubility isotherms from PR + vdW2 and PR + CVD, in terms of $scCO_2$ density and pressure of the system. As can be seen in Fig. 5 (a-d), there are considerable lacks of ability for PR + vdW2 and PR + CVD to be correlated with the experimental data at high and low pressures, respectively. In this regard, the existing deviations in Fig. 5 (d) cause PR + CVD to be not good at all for predicting buprenorphine hydrochloride solubility in $scCO_2$ at temperature of 308 K and pressures below 180 bar. On the other hand, PR + vdW2 exhibits good performance at these conditions, based on Fig. 5 (b).

4.2.2. Correlation results applying density-based models

As mentioned previously, eight density-based models, presented in Table 4, were employed to correlate the experimental solubility data. For this purpose, adjustable parameters were optimized through curve fitting and genetic algorithm in MATLAB software (GA; MATLAB Media).

Table 8 includes the results obtained from correlating the models along with AARD%, R_{adj} , and *F-value* corresponding to each one.

Falling into the range of 17.16%-25.41%, AARD% values indicated acceptable results for correlating the experimental solubility of buprenorphine hydrochloride in scCO₂. With respect to the results, Jouyban and Chrastil models exhibited lowest and highest AARD% with the values of 17.16% and 25.41%, respectively. In addition, Jouyban, Bian and Sodeifian models were better fitted to the experimental data points, exhibiting satisfactory ability for prediction of buprenorphine solubility. As a conclusion, Jouyban model with six adjustable parameters, produced the best results for AARD%, R_{adj} and *Ftest* with the values of 17.16%, 99%, and 89.21, respectively. As expected, Chrastil, Belghit, and Wang models have poorer

Table 9	Approximate values of the total $(\Delta H_{\rm T})$,	vaporization) ΔH_v) and solvation	n (ΔH_s) enthalpies for the in	nvestigated system.
Dissolutio	on of Buprenorphine HCl in scCO ₂	$\Delta H_T(KJ/mol)$	$\Delta H_{v}(KJ/mol)$	$\Delta H_s(KJ/mol)$
		65.594	85.604	-20.010

ability to be correlated with the experimental data rather than the others. It can be resulted from this fact that the mentioned models have lower numbers of adjustable parameters.

To compare calculated theoretical results with experimental data, the correlated solubility isotherms of eight above mentioned density-based models along with experimental data points is depicted in Fig. 6. As can be seen in Fig. 6 (h), Sodeifian's model show higher ability for predicting solubility at higher CO₂ densities. This ability would be resulted from the more number of adjustable parameters in the model (6 parameters, with respect to Table 4), which make it more flexible to be correlated with experimental data. In addition, it should be mentioned that the companion coefficient of each adjustable parameter (e.g., *PlnT* and $ln(\rho T)$ in Sodeifian model) play important roles in this direction. For example, although Belghait model (Fig. 6 (g)) has been developed on the basis of 8 adjustable parameters, it indicated poorer ability for prediction of solubility in scCO₂ compared to Jouyban model (Fig. 6 (e)) that has 6 parameters, because the companion coefficients of Belghait model are not sufficiently correlative for scCO₂-buprenorphine system. The graphical results presented in Fig. 6 (a-h) are in agreement with statistical parameters presented in Table 8.

By applying the correlation results of Chrastil and Bartle models in Eqs. (15) and (16), total ($\Delta H_{\rm T}$) and vaporization enthalpies ($\Delta H_{\rm v}$) for buprenorphine hydrochloride dissolution in scCO₂ can be estimated:

$$\Delta H_{\rm T} = -a_1^{\ Chrastil} R \tag{15}$$

 $\Delta H_{\rm v} = -a_2^{Bartle} R \tag{16}$

Where $a_1^{Chrasil}$ and a_2^{Bartle} are the regressed temperature coefficients of Chrastil and Bartle models, respectively. Considering the difference between the total and vaporization enthalpies, solvation enthalpy of the process (ΔH_s) was also obtained from Eq. (17). These values are reported in Table 9.

$$\Delta H_s = \Delta H_{\rm T} - \Delta H_{\rm v} \tag{17}$$

These enthalpies are of high value for understanding the type and amount of energy needed for solid particles to dissolve in $scCO_2$. For example, a large value of total enthalpy may indicate that solute particles require more energy to dissolve in $scCO_2$ or release more heat when recrystallizing from $scCO_2$. Similarly, the value of vaporization enthalpy would show how strong the intermolecular forces of solute are against $scCO_2$ particles. However, these values have not been directly measured by experiments but were determined based on the assumptions made for developing the utilized semi-empirical models (Sodeifian et al., 2023).

5. Conclusion

To design the pharmaceutical processes such as synthesis of the pharmaceutical micro- and nano particles, drug crystallization, and selective extraction of medicines from mixtures using the supercritical mediums, solubility data of the proposed compound in the fluid are needed. In this research, solubility behavior of buprenorphine hydrochloride in supercritical carbon dioxide (scCO₂) was studied. At the first step, solubility values were measured at different temperatures and pressures over the range of 313-338 K and 120-279 bar, respectively. The highest and lowest equilibrium mole fractions were 4.752×10^{-4} and 0.131×10^{-4} , respectively. The crossover pressure point for this binary system was found to be in the middle of the range of 150-180 bar. At the second step, the obtained solubility data were correlated using Peng-Robinson EoS along with two different mixing rules namely van der Waals type 2 (vdW2) and covolume dependent (CVD) mixing rules. The results showed that Peng-Robinson EoS applied with vdW2 at lower pressures and with CVD at higher pressures could exhibit better capability for correlating the experimental data. In addition to Peng-Robinson EoS, eight different semiempirical density-based models were also examined. Obtaining an AARD% of 17.16 and 18.14, Jouyban and Sodeifian models had better agreement with the experimental data, respectively. At last, by applying the correlation results of Chrastil and Bartle models, total and vaporization enthalpies of buprenorphine hydrochloride dissolution in scCO₂ were estimated to be 65.59 and 85.60 KJ/mole, respectively.

CRediT authorship contribution statement

Gholamhossein Sodeifian: Conceptualization, Methodology, Validation, Investigation, Supervision, Project administration, Writing – review & editing. Maryam Arbab Nooshabadi: Methodology, Investigation, Software, Resources. Fariba Razmimanesh: Methodology, Validation, Writing – original draft. Amirmuhammad Tabibzadeh: Methodology, Validation, Writing – original draft.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgement

The authors appreciate the Research Deputy of University of Kashan for supporting the project financially with the Grant #Pajoohaneh-1401/25. The authors also thank Temad Company for providing the drug required for experimental tests.

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